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FINAL

**INTERMEDIATE AND ALLUVIAL WELL
INSTALLATION REPORT**

SITE 4, EXPLOSIVE WASHOUT LAGOONS

**SUPPLEMENTARY REMEDIAL INVESTIGATION/
FEASIBILITY STUDY OF
UMATILLA DEPOT ACTIVITY
HERMISTON, OREGON**

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LIST OF ACRONYMS AND ABBREVIATIONS

bls	Below land surface
BRAC	Base Realignment and Closure
1,3-DNB	1,3-Dinitrobenzene
2,4-DNT	2,4-Dinitrotoluene
DOT	U.S. Department of Transportation
FSP	Field Sampling Plan
HMX	High Melting Explosive
ID	Inside diameter
NGVD	National Geodetic Vertical Datum
PVC	Polyvinyl chloride
RDX	Royal Demolition Explosive
RI	Remedial Investigation
1,3,5-TNB	1,3,5-Trinitrobenzene
2,4,6-TNT	2,4,6-Trinitrotoluene
UMDA	Umatilla Depot Activity
USAEC	U.S. Army Environmental Center, formerly USATHAMA
USATHAMA	U.S. Army Toxic and Hazardous Materials Agency
XRF	X-ray fluorescence

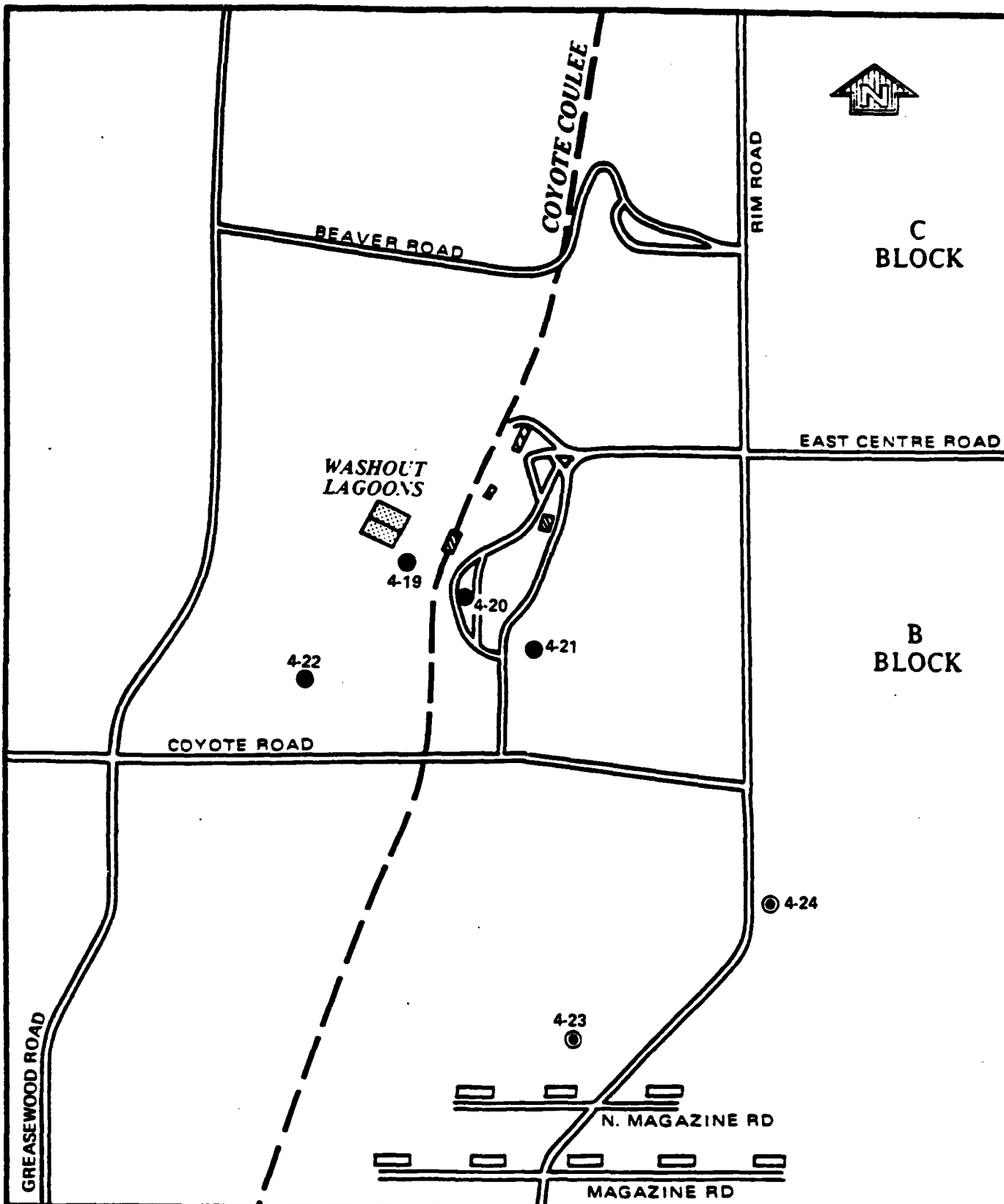
1.0 INTRODUCTION

This report presents the well installation methods and details for four intermediate wells and two alluvial wells installed at Site 4, Explosive Washout Lagoons, Umatilla Depot Activity (UMDA), Hermiston, Oregon. It has been prepared for the U.S. Army Environmental Center (USAEC) formerly the U.S. Army Toxic and Hazardous Materials Agency (USATHAMA), under the Base Realignment and Closure (BRAC) Program, Contract No. DAAA15-90-D-0015, Delivery Order No. 10. The purpose of the report is to document the methods used for the well installations and the hydrogeologic conditions encountered.

As discussed in detail in the Remedial Investigation (RI) report for UMDA (Dames & Moore, 1992b), during previous investigations at Site 4 contamination detected in the unconfined alluvial aquifer was attributed to historical activities at the Explosive Washout Lagoons. Contaminants consist primarily of Royal Demolition Explosive (RDX), High Melting Explosive (HMX), 1,3,5-trinitrobenzene (TNB), 1,3-dinitrobenzene (DNB), 2,4,6-trinitrotoluene (TNT), 2,4-dinitrotoluene (DNT), nitrobenzene, and nitrate/nitrite. Explosives (primarily RDX) and nitrate/nitrite were also detected in deep basalt wells installed into the Columbia River Basalts (4-8, 4-9, 4-10, and 4-17). The nature of the migration pathways for contaminant transport between the alluvial and basalt aquifers was unclear. It was surmised that the migration was facilitated by either natural fracturing within the basalt flows or manmade pathways created during the installation of the four deep wells.

To assist in further evaluating conditions at Site 4, four intermediate monitoring wells--4-19, 4-20, 4-21, and 4-22--were installed as part of the current investigation. The locations of these wells are shown in Figure 1-1. The objectives of the investigation were to:

- Further assess the stratigraphy beneath Site 4.
- Assess the degree of hydraulic interconnection between the basalt and the overlying alluvial sediments.



LEGEND:

- Monitoring Well Completed in Alluvium
- Monitoring Well Completed in First Interbed

0 1000 Feet

**FIGURE 1-1
LOCATIONS OF NEW WELLS**

Dames & Moore

- Document water quality within the intermediate zone between the existing shallow alluvial and deep basalt wells.
- Document horizontal and vertical groundwater flow patterns within the intermediate zone.

In addition, two new alluvial wells--4-23 and 4-24--were installed to the south and southeast of the Explosive Washout Lagoons (see Figure 1-1) to further delineate the extent of explosives and nitrate/nitrite contamination within the alluvial aquifer. Note that the chemical analysis results for the alluvial (as well as intermediate) wells and contamination assessment are presented in an addendum to the RI report.

2.0 INTERMEDIATE WELL INSTALLATION METHODS

2.1 GENERAL WELL INSTALLATION METHODS

The four intermediate wells (4-19, 4-20, 4-21, and 4-22) were installed in accordance with the specifications of the Field Sampling Plan (FSP) Addendum (Dames & Moore, 1992a). The generalized intermediate well construction method is described below and is illustrated in Figure 2-1. Any deviations from the FSP Addendum are also discussed. Boring logs and well construction diagrams for each well are presented in Appendices A and B, respectively.

To minimize the potential of introducing contamination from the alluvial aquifer into the intermediate zone, the boreholes were telescoped at the bedrock contact. A Drill Systems AP-1000 reverse circulation percussion hammer rig was used to penetrate the upper alluvial deposits. An Ingersoll-Rand TH-60 air rotary rig was used to advance the hole in bedrock. In general, the following procedures were used during the drilling and well installation process:

- Triple wall drill casing was driven to refusal with the AP-1000 percussion hammer drill rig. The depth of refusal was between 54.5 and 155 feet below land surface (bls), depending on the well location. The inner dual-wall drill pipe was removed, leaving the 12-inch inside-diameter (ID) steel drill casing in place to prevent the borehole from collapsing. Split-spoon samples were collected at a 5-foot interval for the first well installed (4-19) and a 10-foot interval for the other three wells. As discussed with and agreed to by USAEC, the change from a 5-foot to a 10-foot interval was made primarily because of the homogenous subsurface conditions encountered in the first well and the difficulty in recovery of samples from the cobble-rich matrix of the alluvium.
- The TH-60 air rotary drill rig was moved onto the borehole to advance it into the basalt and to spot core the basalt to verify its nature and composition (see Section 4.3 for a description of this unit, the Elephant Mountain Basalt). An NW size core barrel (2.985 inches by 10 feet in length) was used for spot

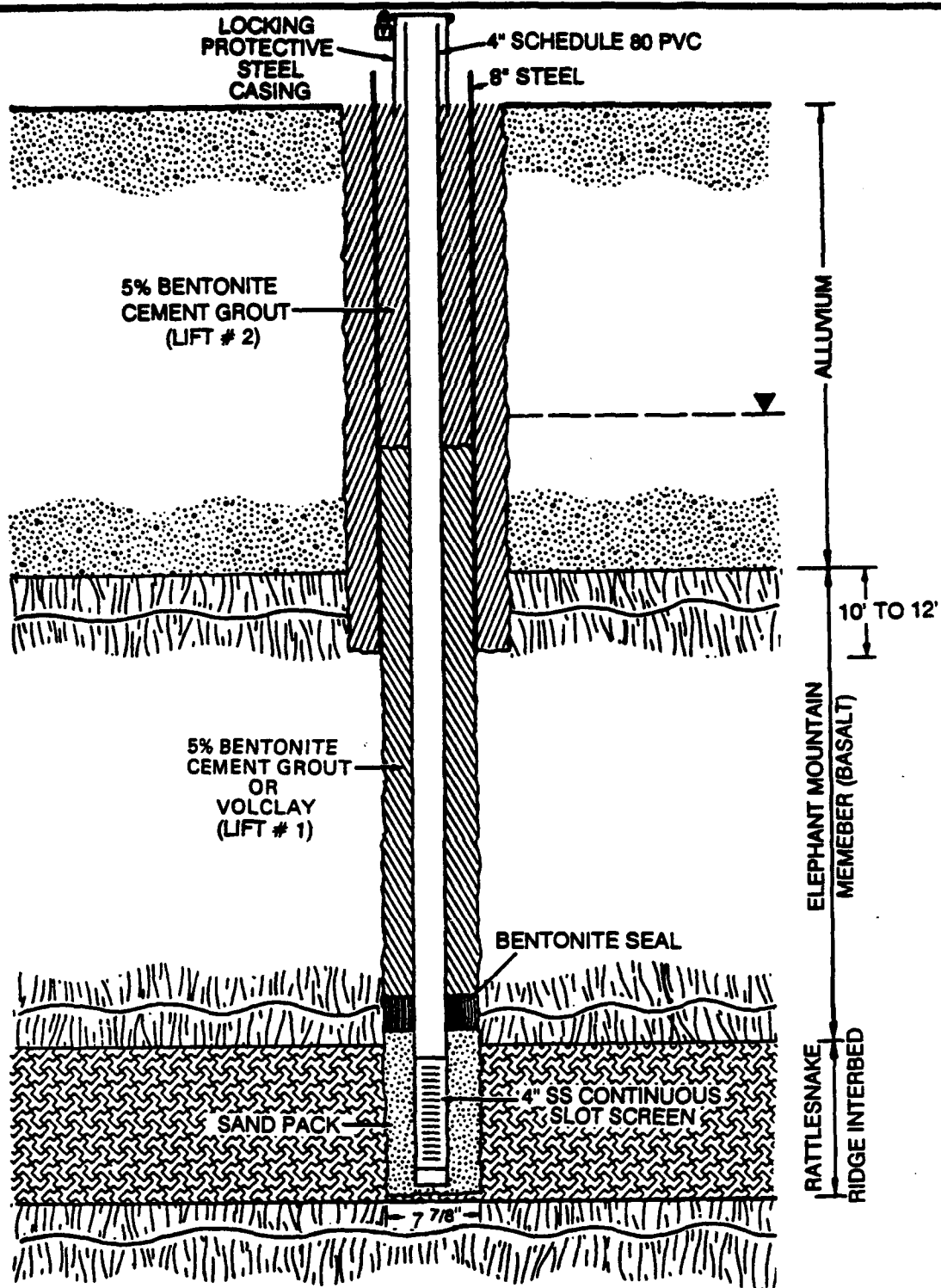


FIGURE 2-1
INTERMEDIATE WELL
CONSTRUCTION DIAGRAM

coring. When core samples were not being collected, a 5 1/2-inch downhole hammer drill bit with reverse air circulation was used to advance the borehole.

- The borehole into the upper basalt was advanced 10 to 12 feet into the unit and then reamed to 10 inches in diameter. An 8-inch steel casing was installed from the surface to 10 to 12 feet into the basalt. This casing was grouted in place using bentonite/cement grout tremied to the bottom of the borehole. The entire annulus was filled with bentonite/cement grout, and a substantial grout plug was tremied inside the 8-inch casing.
- The 12-inch triple wall casing was withdrawn, maintaining a head on the grout in the borehole to preclude collapse of the formation.
- The grout was allowed to cure for at least 12 hours.
- Following the curing period, the grout plug was drilled out and the borehole was advanced to the bottom of the first interbed by direct air rotary methods (see Section 4.3 for a description of this unit, the Rattlesnake Ridge Interbed). During advancement of the borehole, the basalt was spot cored with an NW size core barrel to verify its nature and composition.
- Packer tests were conducted during installation of two of the intermediate wells--4-20 and 4-22. Although not included in the FSP Addendum, as discussed with and agreed to by USAEC, the packer tests were conducted to assess the horizontal permeability of the upper basalt, for which no data were available from previous investigations. In both tests, a single packer was used to isolate a 6-foot interval of basalt within a borehole. Water loss at three pressures was recorded, and horizontal permeabilities were calculated. Data are presented in Appendix C.
- Following the packer test (if it was performed) and prior to installation of the monitoring well casing, the borehole was opened to 7 7/8-inch diameter with the TH-60 air rotary drill rig using a downhole hammer drill bit.

- At the completion of drilling, the drill rig was used to condition the borehole prior to well installation. Borehole conditioning is an important part of the drilling process, because it helps keep the borehole stable and free of obstructions. This was accomplished by slowly moving the drill bit up and down in the borehole while circulating air to remove any dislodged material.
- Monitoring well construction consisted of installing a 4-inch Schedule 80 polyvinyl chloride (PVC) well casing in the borehole. A 10-foot continuously wound stainless-steel well screen (slot size 0.02 inch) was set in the first interbed (150 to 200 feet bls). The continuous slot stainless-steel screen will allow use of any of the intermediate wells as recovery wells if remediation of this interbed is necessary, and if the well locations are consistent with remedial design objectives. A sand pack was placed to 3 to 5 feet above the top of the screen. The filter pack was a 10-20 Colorado Silica sand. A bentonite seal, 3- to 5-feet thick, was placed above the filter sand (Peltonite). Volclay was tremied (in one lift) to the water table in wells 4-19 and 4-21. A 5 percent bentonite/cement grout was tremied to the water table in wells 4-20 and 4-22. This first lift was then allowed to cure. Bentonite/cement grout was tremied from the top of the volclay or grout to the surface in a second lift. The use of volclay was discontinued after wells 4-19 and 4-21 because of the length of time required for it to cure. The long curing time necessitated a 4- to 6-day delay between the first and second grout lifts. While an adequate seal appeared to become established with the volclay, USAEC and Dames & Moore agreed that the 5 percent bentonite/cement grout would be used exclusively in the remaining two wells (4-20 and 4-22), because the faster curing time permitted the second grout lift to be conducted within 12 hours of the first.

Surface completions for all the wells consisted of a protective steel casing over the PVC well casing, four steel pickets, and a gravel blanket. The steel protective casing was 8 inches in diameter and extended approximately 2.5 feet below and 2.5 feet above the ground surface. It was fitted with a sliding steel cap that can be locked to the protective

casing. The steel pickets are 3 inches in diameter and were placed approximately 4 feet from the protective casing. The pickets extend approximately 3 feet below and 3 feet above the ground surface. A 6-inch gravel blanket covered the area between the pickets and the protective casing. A mortar collar was placed inside the protective casing to approximately 6 inches above the ground surface, and a 1/4-inch drainage hole was drilled through the protective casing 1/8-inch above the mortar collar. The protective casing and pickets were painted orange, and the monitoring well's identifying number was painted in white on the protective casing.

All cuttings generated during the drilling activities were placed in new 17H U.S. Department of Transportation (DOT)-certified drums and labeled with well number, date, depth, and contents. Water generated during drilling was contained and transferred to the evaporation basins. The drums of cuttings are being stored in a central area warehouse at UMDA (Building 412) until the start of full-scale remediation of the contaminated soil at the Explosive Washout Lagoons. At that time, the remediation contractor will add the drummed cuttings from the Site 4 wells to the contaminated soil from the lagoons and the material will be composted.

The monitoring wells were developed for approximately 2 hours, between 2 to 7 days after emplacement of the internal mortar collar. Well development was performed using a 5-foot stainless-steel bailer and a submersible pump. The wells were first bailed to help remove any sediment that may have collected in the bottom of the casings. In addition, inserting and removing the bailer created a surging action that helped to clear the well screens. After bailing, the wells were pumped using a submersible pump to complete the development process. Temperature, pH, and conductivity were measured in the water removed from each well at least five times throughout development, always including the first and last water removed from the casings. Field readings collected during well development are provided in Appendix D. Development generally continued until five well volumes--including both the casing and saturated annulus--were removed, the physical parameters were reasonably stable, and the water appeared to be clear. The bailer and submersible pump were steam cleaned between wells; the pump discharge line for each well consisted of dedicated polyethylene tubing.

2.2 WELL-SPECIFIC CONSTRUCTION DETAILS

Table 2-1 summarizes the intermediate well construction. Appendices A and B provide the boring logs and well construction diagrams, respectively. Specific details on the construction history of each of the intermediate wells are as follows:

- Well 4-19 was initiated on 11/11/92. The well was installed on 11/16/92, including the first lift of the volclay. Final surface completion was conducted on 11/20/92. The well was developed on 12/15/92, slug tested on 12/19/92, and groundwater samples collected on 1/8/93.
- Well 4-20 was initiated on 11/30/92. The well was installed on 12/7/92, including the first lift of bentonite/cement grout. Final surface completion was conducted on 12/8/92. The well was developed on 12/18/92, slug tested on 12/19/92, and groundwater samples collected on 1/6/93.
- Well 4-21 was initiated on 11/15/92. The well was installed on 11/19/92, including the first lift of the volclay. Final surface completion was conducted on 11/21/92. The well was developed on 12/16/92, slug tested on 12/19/92, and groundwater samples collected on 1/7/93.
- Well 4-22 was initiated on 12/3/92. The well was installed on 12/9/92, including the first lift of bentonite/cement grout, with final surface completion on 12/10/92. The well was developed on 12/15/92, slug tested on 12/19/92, and groundwater samples collected on 1/9/93.

TABLE 2-1
INTERMEDIATE WELL CONSTRUCTION SUMMARY

Well No.	Surface Elevation (ft)	Measuring Point (msl)	Total Depth (ft)	Depth to Refusal (ft)	Depth of 8" Casing (ft)	Screened Interval (ft)	Screened Interval (msl)	Static Water Level ^{1,2} (ft)	Static Water Elevation ¹ (msl)	Grout Type (first lift)
4-19	557.80	559.59	168.0	94.5	105.0	150-160	407.80-397.80	112.57	445.23	Volclay
4-20	616.40	617.45	218.0	151.0	162.0	198-208	418.40-408.40	145.50	470.90	Volclay
4-21	614.60	616.57	215.0	154.5	167.0	202-212	412.60-402.60	153.92	460.68	Bentonite/ Cement Grout
4-22	514.80	516.58	119.0	55.0	67.0	100-110	414.80-404.80	58.35	456.45	Bentonite/ Cement Grout

¹ Measured December 16, 1992.

² Depth below measuring point (top of casing)

3.0 ALLUVIAL WELL INSTALLATION METHODS

3.1 GENERAL WELL INSTALLATION METHODS

Two alluvial wells (4-23 and 4-24) were installed in accordance with the specifications of the FSP Addendum (Dames & Moore, 1992a). Boring logs and well construction diagrams are presented in Appendices A and B, respectively. A Drill Systems AP-1000 reverse circulation percussion hammer rig was used to penetrate the upper alluvial deposits. The following procedures were employed during the drilling and well installation process:

- Dual-wall drill casing was driven at least 10 feet into the unconfined alluvial aquifer with the AP-1000 percussion hammer drill rig. The depth to the unconfined aquifer was approximately 100 to 103 feet bls, depending on the well locations. Split-spoon samples were collected at selected intervals to verify subsurface lithology.
- Monitoring well construction consisted of installing a 4-inch Schedule 40 PVC well casing in the borehole. A 15-foot cut slot screen (slot size 0.01 inch) was set approximately 10 feet into the water table. A 15-foot screen was used to accommodate seasonal fluctuations of 3 to 5 feet in water table elevations in the unconfined aquifer. The filter pack--a 10-20 CSSI grade Colorado Silica sand--was placed to 5 feet above the top of the screen. A 5-foot-thick bentonite seal was placed above the filter sand (Peltonite). A bentonite/cement grout was tremied from the top of the bentonite grout to the surface.

Surface completions, cuttings disposal, and well development for the two alluvial wells were performed according to the methods described for the intermediate wells in Section 2.1. Figure 3-1 shows the general alluvial well construction details.

3.2 WELL-SPECIFIC CONSTRUCTION DETAILS

Table 3-1 summarizes the alluvial well construction. Appendices A and B provide the well logs and well construction diagrams, respectively. Specific details regarding the construction history of each of the alluvial wells are as follows:

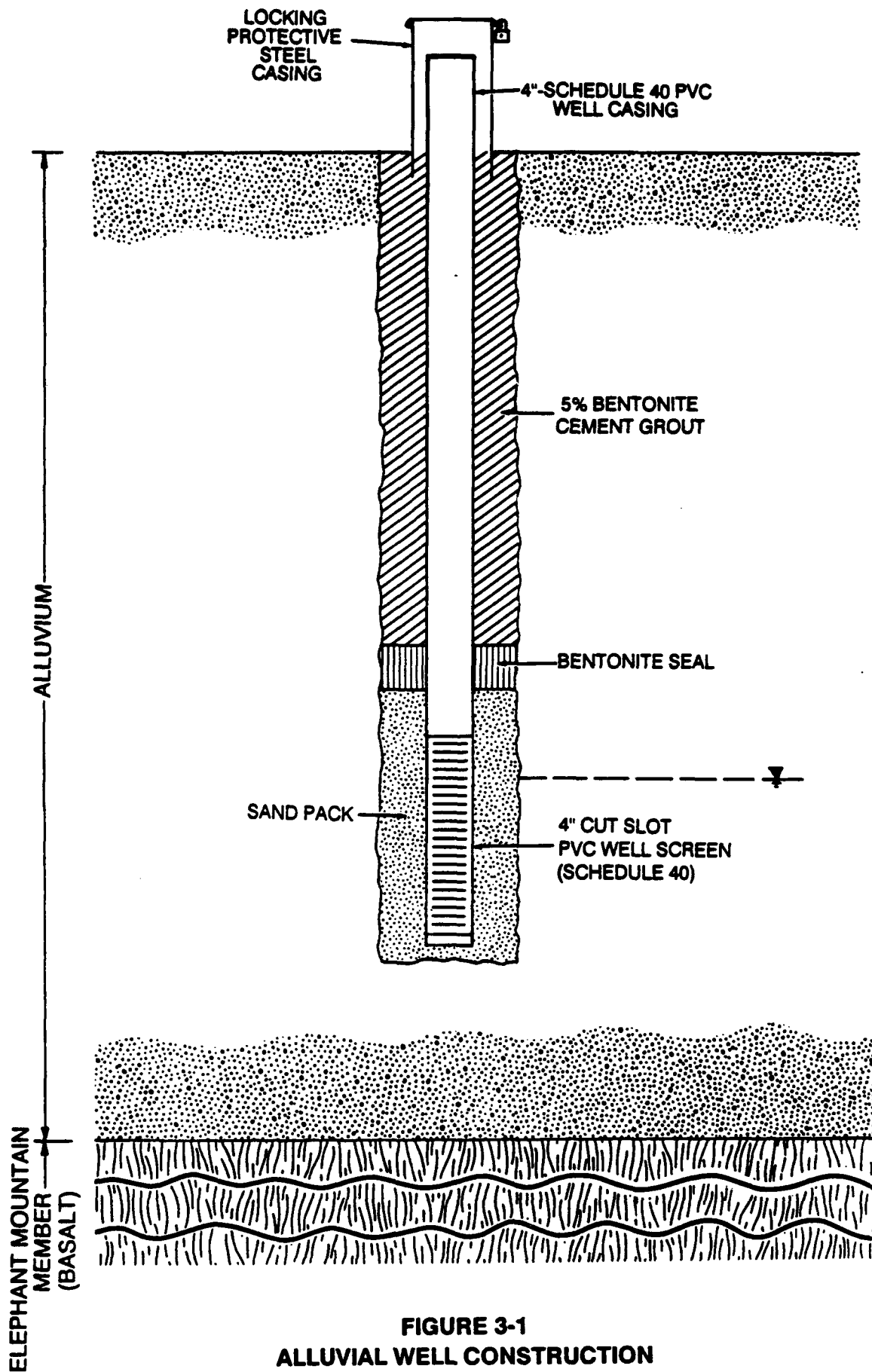


FIGURE 3-1
ALLUVIAL WELL CONSTRUCTION

TABLE 3-1

ALLUVIAL WELL CONSTRUCTION SUMMARY

Well No.	Surface Elevation (ft)	Measuring Point (msl)	Total Depth (ft)	Screened Interval (ft)	Screened Interval (msl)	Static Water Level ^{1,2} (ft)	Static Water Elevation ¹ (msl)
4-23	593.4	595.34	111	94-109	499.4-484.4	100.45	492.95
4-24	596.5	598.15	113.5	96.5-111.5	500.0-485.0	103.45	493.05

¹ Measured December 16, 1992.

² Depth below measuring point (top of casing).

- Well 4-23 was initiated on 11/14/92. The well was installed and completed on 11/15/92. The well was developed on 11/19/92 for a period of 1 hour. Slug testing was conducted on 11/23/92, and groundwater samples were collected on 12/15/92.
- Well 4-24 was initiated on 11/14/92. The well was installed and completed on 11/15/92. The well was developed on 11/19/92 for a period of 1 to 2 hours. Slug testing was conducted on 11/23/92, and groundwater samples were collected on 12/15/92.

4.0 HYDROGEOLOGIC SETTING

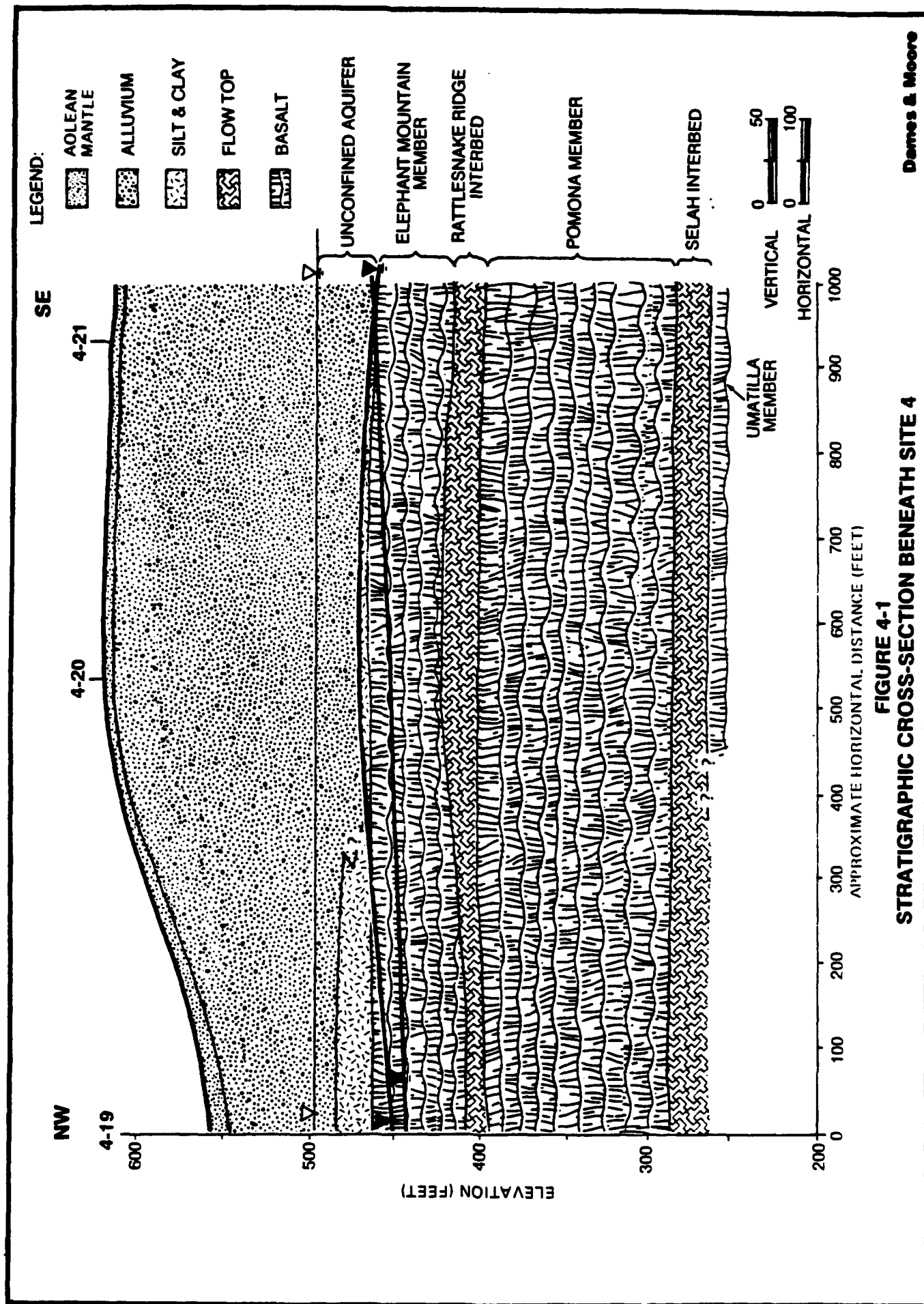
This section describes of the hydrogeologic conditions encountered beneath Site 4 during installation of the four new intermediate wells (4-19, 4-20, 4-21, and 4-22) and the two new alluvial wells (4-23 and 4-24). Also discussed are the hydrogeologic conditions encountered during previous installation of existing wells. Based on the additional data collected during this phase of work, the interpretation of Site 4 geology presented in the 1992 RI report (Dames & Moore, 1992b) has been somewhat revised. Generally, the geologic conditions encountered beneath Site 4 consist of a relatively thin aolean mantle at the surface, Pleistocene alluvial flood deposits, and Miocene basalt flows of the Columbia River Basalts. Figure 4-1 presents a northwest/southeast-trending geologic cross-section through Site 4, based on information from the new and existing wells.

4.1 AOLEAN DEPOSITS

The aolean deposits (windblown sediments) encountered in all new wells varied in thickness from approximately 2 feet (east of Coyote Coulee; see below for description) to 15 feet (west of the Coulee). The aolean mantle consists of a well sorted, fine-to-medium angular sand, tan-to-grey in color. These deposits are similar to those recorded in the boring logs of other Site 4 wells previously installed.

4.2 ALLUVIAL DEPOSITS

The Pleistocene alluvial flood deposits beneath the aolean deposits at Site 4 were deposited by a series of catastrophic flood events, which were precipitated by the cyclic failure and re-building of the ice dams that impounded Glacial Lake Missoula, in western Montana, approximately 17,200 to 11,000 years ago (Breckenridge *et al.*, 1989). Each of these ice dam failures caused extremely high energy flows down the Columbia River. In the area of UMDA, these floodwaters expanded across the Umatilla Basin. Partial constriction of the Columbia River downstream of the Umatilla Basin caused hydrodynamic damming of the floodwaters; formation of glacial Lake Condon; and deposition of significant thicknesses of rounded-to-subrounded sand-, gravel-, and cobble-sized clasts in the Umatilla Basin (Breckenridge *et al.*, 1989). Coyote Coulee, which runs through Site 4 on an approximate northeast/southwest trend, is a 50-foot escarpment interpreted to be formed



by standing waves in the floodwaters. Numerous smaller (10- to 20-foot) bottom ripples are present to the northwest of Site 4 and trend in the same direction.

Geologic samples collected from intermediate wells 4-20 and 4-21, and alluvial wells 4-23 and 4-24, suggest that--to the east of Coyote Coulee--the alluvial flood deposits consist of coarse sands, gravels, and cobbles composed primarily of basalt with lesser amounts of quartz, feldspar, and mica. These deposits extend from the surface (approximately 600 feet above National Geodetic Vertical Datum (NGVD) of 1929) to the basalt contact at approximately 460 feet above the NGVD. Directly above the basalt contact, the sediments are composed of slightly finer saturated silty sands.

Geologic samples from intermediate wells 4-19 and 4-22 suggest that the alluvial flood deposits west of the coulee are typically finer than those to the east, and consist of fine-to-coarse sand and gravel composed primarily of basalt with lesser amounts of quartz, feldspar, and mica. The alluvium extends from the base of the aolean mantle to an approximate elevation of 480 feet above the NGVD, where a sequence of fine sediments approximately 20-feet thick caps the basalt. Sediments are composed of silts, clays, and fine sand, and tend to be dry. At well 4-22, lake varves or rythmites were observed in these sediments, suggesting that they are lacustrine in origin. This unit may represent residual deposits associated with glacial Lake Condon. These lacustrine deposits--which extend to the top of the basalt--remained undisturbed in the lower energy environment on the downstream side of the standing wave associated with later flooding.

The alluvial flood deposits become saturated at approximately 495 feet above the NGVD. The saturated alluvium forms the uppermost aquifer beneath Site 4. It is unconfined, highly permeable, and ranges in saturated thickness from 35 feet (east of the coulee) to 10 to 15 feet (west of the coulee, where the lacustrine deposits thin the alluvium). Previous slug testing and permeability testing suggest a permeability range of 200 to 1,000 feet/day for the alluvium and 3 to 5 feet/day for the silt and clay of the lacustrine deposits (Dames & Moore, 1992b). Slug testing was conducted on the two new alluvial wells (4-23 and 4-24) and analyzed by methods proposed by Bouwer and Rice (1976). Permeability values of 1,571 and 1,944 feet/day, respectively, were obtained (Appendix E).

4.3 BASALT FLOWS

The uppermost basalt flows present beneath Site 4 are those of the Saddle Mountain Formation. Like all the Columbia River Basalts, they erupted during the Miocene Epoch. Flows and interbeds within the Saddle Mountain Formation consist of--from youngest to oldest-- the Elephant Mountain Member, the Rattlesnake Ridge Interbed, the Pomona Member, the Selah Interbed, the Umatilla Member, and the Mabton Interbed (Oberlander and Miller, 1981).

The uppermost basalt flow beneath Site 4 occurs at an approximate elevation of 460 feet above NGVD, or between 50 to 150 feet bls, depending on the location of the well. The topographic surface of the basalt at this area is relatively flat, with a variable depth to basalt due to the topographic expression of Coyote Coulee. Based on installation of the four new intermediate wells, this uppermost flow was found to be approximately 50 to 60 feet in thickness and composed of slightly-to-highly weathered aphanitic light grey basalt. Locally, alteration to kaolanitic clays was observed; however, overall, the rock was only slightly weathered and fractured. X-ray fluorescence (XRF) of core samples collected from this flow during the installation of the intermediate wells was used to evaluate the rock chemistry and identified the flow as the Elephant Mountain Member of the Saddle Mountain Basalts (Beeson, 1993). Results of this analysis are presented in Appendix F.

A flowtop interbed at an elevation of approximately 400 feet was encountered beneath the Elephant Mountain Member; this has been interpreted to be the Rattlesnake Ridge Interbed. The unit is approximately 20-feet thick and is composed of highly chloritized, highly vesicular basalt and interbed sediments. All four intermediate wells (4-19, 4-20, 4-21, and 4-22) were installed into this interbed.

Logs of the previously installed deep basalt wells (4-8, 4-9, 4-10, and 4-17) suggest that a second basalt flow, approximately 100-feet thick, is present beneath the Rattlesnake Ridge Interbed. This flow is interpreted to be the Pomona Member of the Saddle Mountain Basalts. A 20- to 30-foot-thick interbed present beneath this flow is interpreted to be the Selah Interbed. The deep basalt wells are all screened within this interbed.

The Rattlesnake Ridge and Selah Interbeds represent confined or leaky confined aquifers, with the Elephant Mountain and Pomona Members acting as the poorly permeable confining layers that separate them. Packer testing conducted at intermediate wells 4-20 and 4-22 suggest that the horizontal permeabilities in the Elephant Mountain Member range from 0.01 to 0.16 feet/day (Appendix C). Slug testing of the new intermediate wells was conducted and analyzed by methods proposed by Cooper *et al.* (1967). These data suggest that the permeability of the Rattlesnake Ridge Interbed is between 277 and 624 feet/day (Appendix E). Earlier slug testing suggests that the formation permeability of the Selah Interbed is between 2 and 16 feet/day (Dames & Moore, 1992b).

5.0 SUMMARY

Four intermediate and two alluvial wells were installed at Site 4, Explosive Washout Lagoons, at UMDA. Although the geologic conditions encountered were somewhat different from those anticipated, well construction methods were largely in accordance with those presented in the FSP Addendum (Dames & Moore, 1992a). As discussed with and agreed to by USAEC, deviations from this plan included the addition of two packer tests at intermediate wells 4-20 and 4-22; collection of split-spoon samples at 10-foot (rather than 5-foot) intervals at intermediate wells 4-20, 4-21, and 4-22; and use of a bentonite/cement grout mix in place of volclay to seal the borehole annulus beneath the water table at intermediate wells 4-20 and 4-22.

Based on information from the installation of the new wells and existing wells, the geology encountered beneath Site 4 consists of an aolean mantle, alluvial flood deposits, lacustrine sediments in some areas, and basalt flows with associated interbeds. The alluvial flood deposits form a highly permeable but relatively thin unconfined aquifer. The basalt interbeds form a sequence of confined or leaky confined aquifers separated by the basalt flows. The intermediate wells were installed into the uppermost interbed aquifer (Rattlesnake Ridge Interbed).

As discussed in Section 1.0, data were also collected to assess the degree of hydraulic connection between the aquifers, to document water quality within the unconfined alluvial aquifer and Rattlesnake Ridge Interbed, and to document horizontal and vertical groundwater flow patterns. These data are included in an addendum to the RI report.

6.0 REFERENCES

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- Bower, Herman, and R.C. Rice, 1976. "A Slug Test for Determining Hydraulic Conductivity of Unconfined Aquifers With Completely or Partially Penetrating Wells," Water Resources Research, Vol. 12, No. 3.
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- Cooper, H.H., J.D. Biedehoeft, and I.S. Papadopoulos, 1967. "Response of a Finite-Diameter Well to an Instantaneous Charge of Water," Water Resources Research, Vol. 3.
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APPENDIX A

Boring Logs

Dames & Moore

DRILLING CONTR Layne Enl.

No.162879

BY Mark Ochsen

DATE 11/11/92 CHK'D BY

LOCATION OF BORING										JOB NO.		CLIENT		LOCATION	
										06702-086-111		USATHPMA		Umatilla OR	
										DRILLING METHOD: <u>Becker Hammer</u>		BORING NO.		SHEET	
										<u>Reverse Circ.</u>		4-19		1 of 9	
										SAMPLING METHOD: <u>Calif. Split Spoon</u>		DRILLING		START	
										<u>18" x 3" 140# ext. hammer</u>				FINISH	
										<u>30" drop</u>				TIME	
										WATER LEVEL <u>62.64</u>				DATE	
										TIME				1006	
										DATE				DATE	
										CASING DEPTH				11/11/92	
DATUM										ELEVATION		SURFACE CONDITIONS:			
SAMPLER TYPE	INCHES RECOVERED	DEPTH OF CASING, FEET	SAMPLE NO.	BLOWS/FT SAMPLER	NUMBER OF CYCLES	DEPTH IN FEET	SOIL GRAPH	Gently sloping west, sparse vegetation Pred. Sand.							
						0									
						1									
						2									
						3									
						4									
						5									
						6									
						7									
						8									
						9									
						10									
U	18/16	1030	1	10.0	8/19/13	0.0	SP	- Cuttings 0-10': Pinkish-gray f-c sand dry, poorly graded. (Loess deposit?) Micaceous - (Pleistocene)							
						2									
						3									
						4									
						5									
						6									
						7									
						8									
						9									
						10									
U	18/6	1050	2	15.0	9/12/13	0.0	SM	SAND: Pinkish-Gray (7.5YR 6/2), little or no fines, poorly graded sand, damp, Pred. quartz, basalt fine grained, loess deposit, med dense.							
						2									
						3									
						4									
						5									
						6									
						7									
						8									
						9									
						10									
						11									
						12									
						13									
						14									
						15									
						16									
						17									
						18									
						19									
						20									

Dames & Moore

LOCATION OF BORING										JOB NO.		CLIENT		LOCATION	
										06702-08-111		USATHAMA		UMathila, OR	
										DRILLING METHOD:				BORING NO.	
														4-19	
										SAMPLING METHOD:				SHEET	
														2 of 9	
														DRILLING	
										WATER LEVEL				START	
														TIME	
										TIME				TIME	
										DATE				DATE	
										CASING DEPTH					
DATUM										ELEVATION					
SAMPLER TYPE	INCHES DRIVER	DEPTH OF CASING	SAMPLE NO.	BLOWS/FT SAMPLER	NUMBER OF MINUTES	DEPTH IN FEET	SOIL GRAPH	SURFACE CONDITIONS:							
U	18	1100	3	200	4/3/35	0-0	ML SP	SILT: Brown (7.5YR 5/3), <10% v. fine sand, >90% fines, slight plasticity, damp, med stiff, SAND: Pinkish-Gray (7.5YR 6/2), <10% fines, >90% fine sand, poorly graded, damp, loose, Angular Pred quartz & basalt, med dense to dense, micaceous, moist, sand. Occasional fine gravels. (basalt)							
U	18	1120	4	250	5/8/13	0-0	SP	SAND: Pinkish-Gray (7.5YR 6/2), <10% fines, Pred. fine grained sand, poorly graded, damp, loose to med dense, sand is angular, Pred basalt, & quartz. (Salt: Pepper appearance), micaceous, moist-sand. Occasional weathering in sands.							
U	18	1130	5	300	3/15/22	0-0	SM	SILTY SAND: Brown (7.5YR 4/3), 20-25% fines, (non plastic), 75-80% v. fine to fine sand, poorly graded, damp, med. dense, occasional 1/2" later banding, bottom 2" shows oxidation staining (Fe) sand is angular, pred. quartz, feldspar, some basalt, felsic, micaceous, moist sand.							
								-Occasional 2-3" Rounded gravels in Cuttings.							
U	18	1155	6	350	8/15/25	0-0	GP	SANDY GRAVEL: Olive Brown (2.5Y 4/3), <5% fines, 40-45% fine med. sand, 50% gravel, poorly graded, dense, sand is as above, gravel is rounded basaltic and calcl. 1-2",							

See page 1

DRILLING CONTR. Layne Env.

No. 162867

BY Mark Ockner

DATE 11/11/92 CHK'D BY

201 (3) (REV. 11-90)

Dames & Moore

DRILLING CONTR Laurel env.

No. 162868

BY Mark Ochsner

DATE 11/11/92 CHK'D BY

LOCATION OF BORING								JOB NO.		CLIENT		LOCATION			
								06702-086-111		KATHAMA		Umatilla OK			
								DRILLING METHOD:				BORING NO.			
												4-19			
								SAMPLING METHOD:				SHEET			
												309			
												DRILLING			
								WATER LEVEL				START TIME			
								TIME				FINISH TIME			
								DATE				DATE			
								CASING DEPTH							
DATUM								ELEVATION							
SAMPLER TYPE	INCHES DRIVER	INCHES DRIVER	DEPTH OF CASING	SAMPLE NO	BLOWS/FT. SAMPLER	NUMBER OF RINGS	DEPTH IN FEET	SOIL GRAPH	SURFACE CONDITIONS						
U	5"	2"	1210	7	40.0	50-5"	40	GP	SANDY GRAVEL: AS ABOVE						
							1								
							2								
							3								
							4		- 1-3" Rounded gravels (basalt) in Sand matrix in cuttings Rounded to Subrounded.						
							4.5	SP/GP	SANDY GRAVEL: Brown (10YR 5/3), ~50% fine to med Sand, ~50% gravel, poorly graded, damp, little or no fines < 5%, dense, Sand is rounded to Subrounded.						
U	12"	6"	1230	8	45.0	50-6"	6		Med. quartz: basalt, felsic, gravel is subrounded basaltic & slightly weathered, micaceous						
							7								
							8								
							9								
							50	GW	GRAVEL: Grayish Brown (10YR 5/2), 5-10% fine to coarse Sand, well graded, angular basalt fragments, fine med. basalt, quartz, damp, med dense						
							1	SP	SAND: Brown (10YR 5/3), 5% fines, med fine Sand, poorly graded, damp						
U	18"	18"	1240	9	50.0	18-22"	1	GW	SILT: Brown (10YR 5/2), slightly plastic SILT, 5% v. fine Sand.						
							2		GRAVEL: Grayish Brown (10YR 5/2), 5-10% fine to coarse Sand, well graded, moist, med dense, gravel is angular, med basalt, quartz, & spar						
							3								
							4								
							53	GP	GRAVEL: Dr. Grayish Brown (10YR 4/2), < 5% fines, med. fine, angular to subrounded basalt, some quartz & Volcanics, poorly graded, damp, med dense.						
U	18"	18"	1310	10	55.0	18-21"	6		< 10% fine to coarse Sand, gravel is slightly to med. weathered.						
							7								
							8								
							9								
							60								

Dames & Moore

[illegible]

Dames & Moore

LOCATION OF BORING										JOB NO.		CLIENT		LOCATION					
										06702-086-111		USATHAMA		Umatilla, OR					
										DRILLING METHOD:				BORING NO.					
										Air Rotary TH-60				4-19					
										94.5' →				SHEET					
										See Page 1				5 of 9					
										SAMPLING METHOD:				DRILLING					
														START					
										WATER LEVEL				TIME					
										TIME				TIME					
										DATE				DATE					
										CASING DEPTH									
DATUM										ELEVATION									
SAMPLE TYPE	INCHES RECOVERED	DEPTH OF CASING	SAMPLE NO.	BLOWS/FT	NUMBER OF SAMPLES	DEPTH IN FEET	SOIL GRAPE	SURFACE CONDITIONS											
U	18 1/4	1500	15 1/2	1/16	0.0	80	ML/SM	SANDY SILT: GRAY (SY SLI) 30-35% v.f. Sand, 65-70% fines, slightly plastic, med. stiff to stiff, moist - not saturated.											
						81													
						82													
						83													
						84													
						85	GM	SILTY SANDY GRAVEL: GRAY (SY SLI), 20-25% fines, 30% f.m. angular sand, 45% f.c. gravel, poorly graded, saturated, v. dense, gravel is angular to subrounded basalt, slightly weathered, sand is pred. felsic, quartz, ksp. basalt. Several pieces of cemented ash - tuff?											
						86		- harder drilling at 86.0'											
						87													
						88													
						89													
						90	CL/ML	CLAYEY SILT: v. pale brown (10YR 7/2), 15% v. fine sand, pred. 100% fines, slight plasticity, med-stiff, damp - not saturated, cohesive											
						91		end of day											
						92													
						93		Refusal at 94.5' bgs w/ Becker Hammer 08:55											
						94		Air rotary begins w/core (NW) 2985" x 10' barrel.											
						95	B	BASALT: (95-102.5' core): DK GRAY (7.5YR 4/0), slightly weathered, vesicular basalt, weathered horizontal fracturing, traces of fine sand, rare secondary calcite filling, no phenocrysts, no pyrite, no vertical fracturing, chlorite in one vesicle, yellow-brown color in horiz. fractures - hematite. not saturated											
						96		ROD = 29% Recovery = 88%											
						97													
						98													
						99													
						100													

See Page 1

DRILLING CONTR. Layne Engr.

No. 162898

BY Mark Ochsner

DATE 11/11/92 CHK'D BY

088.1 (3) (REV. 11-88)

core run #1
95-102.5'

Dames & Moore

DRILLING CONTR Layne env.

No.162900

BY Mark Ochsner

DATE 11/14/92 CHK'D BY

0201 (2) (REV. 11-80)

LOCATION OF BORING										JOB NO. 06702-006-111		CLIENT USATAMA		LOCATION Umatilla OK			
See Page 1										DRILLING METHOD:				BORING NO. 4-19			
										See Page 1				SHEET 6 of 9			
														DRILLING			
														START TIME	FINISH TIME		
DATUM										ELEVATION				CASING DEPTH		DATE	
SAMPLER TYPE	INCHES DRIVEN RECORDED	DEPTH OF CASING	SAMPLE NO.	BLOWS/FT SAMPLER	NUMBER OF RINGS	DEPTH IN FEET	SOIL GRAPH	SURFACE CONDITIONS.									
						100		BASALT: core run #1 95-102.5' AS Above									
						1											
						2											
						3											
						105	B	- Cuttings are dry, lt brown sand - probably rock flour - hard drilling 13 min/ft. - B" casing set increment from surface to 105'									
						6											
						7											
						8											
						110	B	- V. hard drilling - 15:16 ^{min} /ft									
						1											
						2											
						3											
						115	B	BASALT: GRAY (7.5YR 4/6), moderately weathered vesicular basalt, Aphanitic, some mafic minerals, with CA & Plag (An 50%), no phenocrysts, some vertical fracturing - closed to staining, horizontal fracturing, occasional secondary mineralization of vesicles & fractures. RQD = 50% Recovery = 100% Core terminated at 117.5' due to slow penetration.									
						6											
						7											
						8											
						120											

Dames & Moore

DRILLING CONTR. Large Env.
No. 162886

BY Mark Ackner
DATE 11/15/92 CHK'D BY

800.1 (2) (REV. 11-90)

LOCATION OF BORING						JOB NO.		CLIENT		LOCATION			
See Page 1						06702-086		USATHAMA		CMAA/LLA OK			
						DRILLING METHOD:						BORING NO.	
						See Page 1						419	
												SHEET	
												7 of 9	
SAMPLING METHOD:						DRILLING							
WATER LEVEL						START		FINISH					
TIME						TIME		TIME					
DATE						DATE		DATE					
CASING DEPTH													
DATUM						ELEVATION							
SAMPLER TYPE	INCHES DEPTH	INCHES DEPTH	DEPTH OF CASING	SAMPLE NO	BLOWS/FT SAMPLER	NUMBER OF RINGS	DEPTH IN FEET	SOIL GRAPH	SURFACE CONDITIONS:				
							120	B	V. Hard drilling - Blue gray dust coming from cyclone - basalt approx. 15 min./ft				
							1						
							2						
							3						
							4						
							5						
							6						
							7						
							8						
							9						
							130		- Begin CORE RUN #3 from 130-134'				
							1		BASALT: GRAY (7.5 YR 5b), Highly vesicular, mod. weathered basalt. High Alteration of basalt in places to kaolinite. TOP 1 foot of core has completely weathered basalt to clay (yellow brown), horizontal fracturing, vesicles completely filled with secondary minerals, no phenocrysts, secondary minerals are pred chlorite, basalt is aphanitic, some ca. plag is visible in mafic matrix. RAO: 1906 Leidenberg - 42%				
							2						
							3						
							4						
							5						
							6		V. hard drilling - blue gray cuttings, basalt				
							7						
							8		Easier drilling and some H ₂ O at 138'. Probably weathered fracturing in basalt.				
							9						
							140						

Dames & Moore

by Mark Ochsnor

No. 162887

DRILLING CONTR

DATE 11/15/92 CHK'D BY

688.1 (2) (REV. 11-90)

LOCATION OF BORING						JOB NO.		CLIENT		LOCATION			
<div style="position: relative; height: 100px;"> See Page 1 </div>						0662086-11		USATHAMA		Umatilla OR			
						DRILLING METHOD:						BORING NO.	
						<div style="position: relative; height: 100px;"> See Page 1 </div>						4-19	
												SHEET	
												8-9	
SAMPLING METHOD:						DRILLING							
WATER LEVEL						START		FINISH					
TIME						TIME		TIME					
DATE						DATE		DATE					
CASING DEPTH													
DATUM						ELEVATION							
SAMPLER TYPE	INCHES DOWN	INCHES RECOVERED	DEPTH OF CASING	SAMPLE NO	BLOWS/FT SAMPLER	NUMBER OF RINGS	DEPTH IN FEET	SOIL GRAPH	SURFACE CONDITIONS:				
							40	B	V. Hard drilling - occasional water in cyclone - from 135-138' 13 min/ft.				
							1						
							2						
							3						
							4						
							5						
							6						
							7						
							8	ML	- Blue gray cuttings - basalt fragments.				
							9						
							10						
							150	B	SANDY SILT: Blue Gray (56 G/I), 25% v. fine sand, 75% fines, slightly plastic, moist, stiff. Probably completely weathered basalt.				
							1						
							2						
							3						
							4						
							5						
							6						
							7						
							8		BASALT: GRAY (7.5% S/O), highly vesicular basalt, mod. to highly weathered, several zones of chlorite fillings, some pyrite inclusions, fractures and fillings vesicles are open, color is distinctly blue/greenish gray. Rock is aphanitic mafic matrix, no phenocrysts, RQD = 72% Recovery = 90%				
							9						
							10						
							11						
							12						
							13						
							14						
							15						
							160		- Probable flow top. Contact between Pampa and Umatilla members - Selah Interbed?				
							1						
							2						
							3						
							4						
							5						
							6						
							7						

core run #4
150-160

Dames & Moore

See Page 1					JOB NO. 06702-086-11		CLIENT USATAMA A		LOCATION Umatilla OK			
					DRILLING METHOD:						BORING NO. 419	
					SAMPLING METHOD: See Page 1						SHEET 9 of 9	
					WATER LEVEL						DRILLING	
					TIME						START TIME	
DATE						FINISH TIME		DATE				
CASING DEPTH						DATE		DATE				

DATUM				ELEVATION					
SAMPLER TYPE	INCHES DRIVER INCHES RECORDED	DEPTH OF CASING	SAMPLE NO	BLOWS/FT SAMPLER	NUMBER OF RINGS	DEPTH IN FEET	SOIL GRAPH	SURFACE CONDITIONS	
				Core run #5	160-168'	6	B	<p>BASALT: Lt Gray (7.5YR 6/6), relatively competent basalt, Aphanitic mafic matrix. Secondary minerals of chlorite + calcite in vesicles, no phenocrysts, occasional vesicles, fewer than above. Fractured zone at 162'</p> <p>- Basalt is more competent w/ depth beneath flow top.</p>	
						1			
						2			
						3			
						4			
						5			
						6			
						7			
						8			
						9			
						10		<p>Boring terminated at 168' bgs. on 11/15/92 G.W. encountered at 162-164' during drilling</p>	
						1			
						2			
						3			
						4			
						5			
						6			
						7			
						8			
						9			
						10			
						1			
						2			
						3			
						4			
						5			
						6			
						7			
						8			
						9			
						10			

No. 162873
 DRILLING CONTR. Leysen Saw.

BY Mark Olsner
 DATE 11/15/92 CHK'D BY

Dames & Moore

LOCATION OF BORING										JOB NO.		CLIENT		LOCATION			
										06702081-11		USATHAWA		UMATILLA, OR			
										DRILLING METHOD: Becker Hammer						BORING NO.	
										Percussion, reverse air						4-20	
										Triple and 659 12" 9" 6"						SHEET	
										SAMPLING METHOD:						1 of 11	
Calif Split Spear 3" x 18"										DRILLING							
140# ext. hammer 30" drop										START TIME		FINISH TIME					
WATER LEVEL										1020							
TIME										DATE		DATE					
CASING DEPTH										11/30/92							
SURFACE CONDITIONS:																	
Relatively Flat Sand : Brush area																	
SAMPLER TYPE	INCHES DRIVEN	INCHES RECOVERED	TIME SAMPLED	SAMPLE NO.	BLOWS/FT	SAMPLER	CUMULATIVE BLOWS	DEPTH IN FEET	SOIL GRAPE								
								0									
								1									
								2									
								3	SP	SAND: Reddish Brown (7.5R 4/3), micaceous, angular quartz; basalt - cuttings - dry							
								4									
								5									
								6									
								7		- fine-med rounded gravels - basalt in sandy matrix - dry							
								8									
								9									
								10	GP	SANDY GRAVEL: DK Brown (7.5R 4/2), 65-10% fines, 30-35% m-c Sand - angular quartz, basalt, 65-70% f-m gravels, rounded, basalt clasts in sandy matrix, poorly graded, dry, Grab Sample - no split spear							
Grab	-	10:30	10.0	-	0.0			1									
								2									
								3									
								4									
								5									
								6	GP	- Sandy Gravel as above							
								7									
								8									
								9									
								20									

DRILLING CONTR Lapee Env.

No.161972

BY Mark Ackner
DATE 11/30/92 CHK'D BY

006.1 (3) (REV. 11-00)

Dames & Moore

LOCATION OF BORING				JOB NO.	CLIENT	LOCATION
				06702-086-111	USA THAMA	Umatilla OR
<div style="font-size: 2em; transform: rotate(-15deg); position: absolute; top: -50px; left: 100px;">See Page 1</div>				DRILLING METHOD:		BORING NO. 4-20
				SAMPLING METHOD: See Page 1		SHEET 2 of 11
				WATER LEVEL		START TIME
				TIME		FINISH TIME
				DATE		DATE
				CASING DEPTH		

DATUM	ELEVATION	SAMPLER TYPE	INCHES DRIVEN	INCHES RECORDED	FEET TO BOTTOM	CASING	SAMPLE NO.	GLOWS/FT SAMPLER	CUMULATIVE NUMBER OF GLOWS	DEPTH IN FEET	SOIL GRAPH	SURFACE CONDITIONS:
		U	18"	1045	2'	11/24	0.0			2.0	GP	SANDY GRAVEL: Dk Grayish-Brown (over 5%), <5% fines, 15-20% f-c Sand - angular basalt: quartz, mafic, 75-80% f-c gravels, subrounded to rounded basalt clasts, fresh, poorly graded, dry, occasional mica in sand, dense.
										1		
										2		
										3		
										4		
										5		- Sandy Gravel - as above
										6		
										7		
										8		
										9		
		U	5' / 3"	1110	3'	30-0	905"	0.0		30	GP	GRAVEL: Gray (7.5YR 5/6), little or no fines, 100% angular basalt, fractured by split spalls, dry basalt cobbles, v. dense.
										1		
										2		
										3		
										4		
										5	GP	- increase in Sand (m-z), cuttings became Sandy Gravel.
										6		
										7		
										8		
										9		
										40		

Dames & Moore

No. 162877 DRILLING CONTR. Layne Env.

BY Mark Ochsner
DATE 11/30/92 CHK'D BY

LOCATION OF BORING						JOB NO.		CLIENT		LOCATION			
See page 1						0702-08-11		USATHAMLA		Umatilla OK			
						DRILLING METHOD:						BORING NO.	
						See Page 1						4-20	
						SAMPLING METHOD:						SHEET	
												3 of 11	
DATUM						ELEVATION		WATER LEVEL		DRILLING			
								TIME		START			
								DATE		TIME			
						CASING DEPTH		DATE		DATE			
SAMPLER TYPE	INCHES RECOVERED	DEPTH OF CASING	SAMPLE NO.	BLOWS/FT SAMPLER	NUMBER OF RINGS	DEPTH IN FEET	SOIL GRAPH	SURFACE CONDITIONS:					
U	4" 4"	1130	34 40	50-9"		40	GP	SANDY GRAVEL: Dk Grayish Brown (10 YR 5/2), < 5% fines, 20-25% F-C Sand (angular basalt gravel), 70-75% F-C Gravels, poorly graded, dry, v. dense, gravel is angular to subrounded basalt clasts. Nose of sampler plugged w/ basalt.					
						1							
						2							
						3							
						4							
						5		- Cuttings as Above					
						6							
						7							
						8							
						9							
U	18 12	1200	5 500	37/41 48		50	GP	SANDY GRAVEL: GRAY (7.5 YR 5/6), < 5% fines, 10-15% f-c Sand, angular, pred basalt (ma fel), 85-90% f-c gravel, pred angular basalt, some rounded pieces, poorly graded, dry, v. dense.					
						1							
						2							
						3							
						4							
						5		- drilling harder at 56' bgs. Coarse gravels to cobbles in cuttings.					
						6							
						7							
						8							
						9							
						60							

Dames & Moore

DRILLING CONTR. Cayce, Ind.
No. 162876

BY Mark Ochsen
DATE 11/20/92 CHK'D BY
620.1 (2) (REV. 11-90)

LOCATION OF BORING										JOB NO. <u>0602-026-111</u>		CLIENT <u>KATHANA</u>		LOCATION <u>Mattila OK</u>			
<div style="text-align: center; font-size: 2em;">See Page 1</div>										DRILLING METHOD:				BORING NO. <u>4-20</u>			
										SAMPLING METHOD: <u>See Page 1</u>				SHEET <u>7 of 11</u>			
										WATER LEVEL				START TIME		FINISH TIME	
										TIME				DATE		DATE	
DATUM										ELEVATION							
SAMPLER TYPE	INCHES RECORDED	DEPTH OF CASING	SAMPLE NO.	BLOWS/FT SAMPLER	NUMBER OF RINGS	DEPTH IN FEET	SOIL GRAPH	SURFACE CONDITIONS:									
U	6"	1300	6	50-6"		60	GP	<p>SANDY GRAVEL: Gray (7.5YR 5/0), < 5% fines, 15-20% f-c angular sand, med. basalt, quartz, 20-25% f-c gravels, angular basalt, poorly graded, dry, v. dense, occasional basalt cobbles in clittings at 60'</p> <p>- occasional basalt cobbles in cyl. core (4 to 6")</p>									
						1											
						2											
						3											
						4											
						5											
						6		<p>SANDY GRAVEL: DE GRAYISH BROWN (10YR 5/2), < 5-10% fines, 20-35% f-c sand (angular basalt, quartz), 60-65% gravel, poorly graded, dry, dense, gravel is surrounded by angular basalt clasts, some quartzite, limestone, f-c gravel.</p> <p>- gravels become finer, rounder</p> <p>- increase in sand - highly mafic. m-c sand in cut as</p>									
						7											
						8											
						9											
						10											
						11											
						12		<p>- increase in sand - highly mafic. m-c sand in cut as</p>									
						13											
						14											
						15											
						16											
						17											
						18		<p>- increase in sand - highly mafic. m-c sand in cut as</p>									
						19											
						20											
						21											
						22											
						23											
						24		<p>- increase in sand - highly mafic. m-c sand in cut as</p>									
						25											
						26											
						27											
						28											
						29											
						30		<p>- increase in sand - highly mafic. m-c sand in cut as</p>									
						31											
						32											
						33											
						34											
						35											

Dames & Moore

DRILLING CONTR. Layne, Inc.

No. 162875

BY Mark A. Schner

DATE 11/30/92 CHK'D BY

QSS-1 (3) (REV 11-90)

LOCATION OF BORING										JOB NO.		CLIENT		LOCATION							
See Page 1										16702-006-711		USATHAMA		MATHILAK OK							
										DRILLING METHOD:										BORING NO.	
										See Page 1										4-20	
																				SHEET	
										SAMPLING METHOD:										5 of 11	
WATER LEVEL										START		FINISH									
TIME										TIME		TIME									
DATE										DATE		DATE									
CASING DEPTH																					
DATUM										ELEVATION		SURFACE CONDITIONS:									
SAMPLER TYPE	INCHES DRIVEN	INCHES RECORDED	DEPTH OF CASING	SAMPLE NO.	BLOWS/FT	SAMPLER	NUMBER OF	DEPTH IN FEET	SOIL NAME												
U	18	16	130	8	8/31/50	0.0	80	GW	SANDY GRAVEL: Dk Grayish Brown (10YR 5/2), 5-10% fines, 25-30% f-c sand (angular basaltic, some quartz & fsp), 70-75% gravels, angular to subrounded, basalt, some quartzite, fine to coarse well graded, dry, dense.												
								1													
								2													
								3													
								4													
								5		- Gravel becomes finer - well rounded											
								6													
								7													
								8													
								9													
U	18	14	30	9	8/31/50	0.0	90	GP	SANDY GRAVEL: Dk Grayish Brown (10YR 5/2), < 5-10% fines, Basalt Recovered 2-4 basalt fragments, dry basalt casing returns at 50' indicate 25-30% m-c sand, angular basalt, quartz, 70-75% f-c gravels, basalt, angular to sub rounded, poorly graded, damp, dense.												
								1													
								2													
								3													
								4													
								5		- cuttings are as above - Sandy Gravel											
								6		dry											
								7													
								8													
								9													
								10													

Dames & Moore

See Page 1		LOCATION OF BORING		JOB NO. 06702086-111	CLIENT VIA THANA	LOCATION Kamathik OR	
		DRILLING METHOD:				BORING NO. 420	
		SAMPLING METHOD:				SHEET 6 of 11	
		WATER LEVEL				DRILLING	
		TIME				START TIME	
DATE				DATE		FINISH TIME	
CASING DEPTH				DATE			

DATUM		ELEVATION		SURFACE CONDITIONS:	
SAMPLER TYPE	INCHES DRIVER	INCHES RECORDED	INCHES CASTING	SAMPLE NO	DEPTH IN FEET
U	12	1515	10	23	0.0
					1
					2
					3
					4
					5
					6
					7
					8
					9
U	0	1600	11	50	110
					1
					2
					3
					4
					5
					6
					7
					8
					9
					10
					11
					12

GP SANDY GRAVEL: DE GRAYISH BROWN (CORE 5/2), <5% fines, 20-25% f-c Sand, granular, no silt; Gravel, (Chitic), 75-80% f-c gravel, angular to subrounded Basalt, fresh, poorly graded, damp, v. dense.

- Sandy Gravel as above - dry

GP NO Recovery at 110' - Casing returned at 110' exhibits Sandy Gravel as above, dry

end of day

- Cuttings are as above

DRILLING CONTR. Layne-Guth
No. 161904

BY Mark Ochsner
DATE 11/30/92 CHK'D BY

000 1 (2) (REV. 11-90)

Dames & Moore

DRILLING CONTR Layne Env.
No. 161906

BY Mary Schoener
DATE 12/1/97 CHK'D BY

000.1 (2) (REV. 11-90)

LOCATION OF BORING										JOB NO.		CLIENT		LOCATION					
See Page 1										06702-086-111		USATHAMA		UNMATHA OK					
										DRILLING METHOD:				BORING NO.					
														4-20					
										SAMPLING METHOD:				SHEET					
														7 of 11					
										DRILLING		START		FINISH					
										WATER LEVEL				TIME		TIME			
										TIME									
										DATE				DATE		DATE			
										CASING DEPTH									
DATUM										ELEVATION									
SAMPLER TYPE	INCHES BITTER	INCHES WHEEL	INCHES CASING	SAMPLE NO	BLOWS/FT	DEPTH IN FEET	SOIL GRAPH	SURFACE CONDITIONS:											
60ab	-	0730	12	120	-	0.0	20	GP	SANDY GRAVEL: DE Grayish Brown (10YR5/2), 1-5% fines, 25-30% f-m sand-angular quartz, 1/8 to 1/4" size, 10-15% f-c gravel - angular, to subrounded basalt clasts, dry, poorly graded, appears dense.										
							1												
							2												
							3												
							4												
							5												
							6												
							7		- cuttings became saturated at 127'										
							8												
							9												
4	0"	0900	13	130	50-0'	0.0	130	GP	NO Recovery: casing returns are SANDY GRAVEL as above saturated.										
							1												
							2												
							3												
							4		- occasional 4-6" cobbles in cyclone rounded, saturated.										
							5												
							6												
							7												
							8												
							9												
							10												

Dames & Moore

DRILLING CONTR. Layne-Gull.
No. 161908

BY Mark Adelman
DATE 12/19/72 CHK'D BY

080.1 (2) (REV. 11-66)

LOCATION OF BORING										JOB NO.		CLIENT		LOCATION			
<div style="position: absolute; top: 100px; left: 100px; font-size: 2em; transform: rotate(-15deg);">See Page 1</div>										06702-086		USATHAMA		CMACTILLA DE			
										DRILLING METHOD:				BORING NO.			
										Air Rotary TH to from 151.0'				4-20			
										5 1/2 inch hole hammer				SHEET			
										SAMPLING METHOD:				8 or 11			
NW Core barrel 2.925" x 10'										DRILLING							
WATER LEVEL										START TIME		FINISH TIME					
TIME										DATE		DATE					
DATE										CASING DEPTH							
DATUM										ELEVATION							
SAMPLE TYPE	INCHES DEPTH	INCHES DEPTH	INCHES DEPTH	INCHES DEPTH	INCHES DEPTH	INCHES DEPTH	INCHES DEPTH	INCHES DEPTH	INCHES DEPTH	DEPTH IN FEET	SOIL GRAPH	SURFACE CONDITIONS					
U	0"	0"	1000'	14'	50-0"	0.0				140	GP	NO Recovery at 140' : cuttings are sandy GRAVEL - As above, saturated.					
										1							
										2							
										3							
										4							
										5							
										6							
										7							
										8							
										9							
										10							
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										100							

Dames & Moore

DRILLING CONTR Layne Inc.

No. 161909

BY Mark Olsner
DATE 12/16/92 CHK'D BY

928.1 (31) (REV. 11-90)

LOCATION OF BORING										JOB NO.		CLIENT		LOCATION							
<p style="font-size: 2em; transform: rotate(-15deg);">See Page 1</p>										06702-086-111		USATHAMA		Umatilla OR							
										DRILLING METHOD:										BORING NO.	
										Air Rotary - TH 60										4-20	
										5 1/2" D.H. Hammer										SHEET	
										SAMPLING METHOD:										9 & 11	
NW Core barrel 2.985" x 10'										DRILLING		START		FINISH							
WATER LEVEL										TIME		DATE		DATE							
TIME										DATE		DATE		DATE							
DATE										DATE		DATE		DATE							
CASING DEPTH										DATE		DATE		DATE							
DATUM										ELEVATION		SURFACE CONDITIONS:									
SAMPLER TYPE	INCHES DRIVEN INCHES RECOVERED	DEPTH OF CASING	SAMPLE NO.	DEPTH	BLOWS/FT SAMPLER	NUMBER OF HITS	DEPTH IN FEET	SOIL GRAPH													
							160	B	Core run #1 157-162'												
							1														
							2		Set 8" steel casing to 162.0'												
							3		end of day												
							4		- 13' of leave in hole - Switch to Becker hammer												
							5		and re-drive 12" csq. Flush-hole. Hole												
							6		cleaned to 160'. no leave in hole.												
							7														
							8														
							9														
							170	B	BASALT: Lt Gray (10YR 6/6), highly fractured,												
							1		slight to med. weathered basalt, Fe staining												
							2		upper 2-3' of core. Basalt becomes slightly												
							3		vesicular, (weathered-out minerals), slightly												
							4		weathered basalt, more competent rock at 175.												
							5		RQD = 59% Recovery: 60%												
							6		Good water return at 170'. Basalt becomes												
							7		dry at 172-173'												
							8														
							9														
							176 1/2	B	BASALT: Lt Gray (10YR 6/6), aphanitic, slightly												
							1		vesicular, slightly weathered basalt, competent												
							2		Rock, some horizontal fracturing w/ Fe staining.												
							3		Some secondary minerals of olivine present.												
							4		RQD = 57% Recovery: 78%												
							5														
							6														
							7														
							8														
							9														
							180														

Drilling Contra Layne Ind.

No.161842

Mark Johnson
1246/92

DATE 1/16/92 CHK'D BY

A-20

Dames & Moore

No. 161843 DRILLING CONTR Wayne Eng.

BY Mark Johnson
DATE 12/6/92 CHK'D BY _____

680.1 (2) (REV. 11-80)

LOCATION OF BORING										JOB NO. <u>6602-086-111</u>		CLIENT <u>USATHAMA</u>		LOCATION <u>Wunatilla OK</u>					
See Page 1										DRILLING METHOD:				BORING NO. <u>4-20</u>					
										See Page 1				SHEET <u>11 of 11</u>					
										SAMPLING METHOD:				DRILLING					
										WATER LEVEL				START TIME		FINISH TIME			
TIME				DATE				DATE											
CASING DEPTH				DATE				DATE											
DATUM										ELEVATION									
SAMPLER TYPE	INCHES DRIVEN RECORDED	DEPTH OF CASING	SAMPLE NO. DEPTH	BLOWS/FT SAMPLE	NUMBER OF MIN'S	DEPTH IN FEET	SOI GRAPH	SURFACE CONDITIONS:											
						20		See Page 1											
						1		Basalt cont'											
						2													
						3													
						4													
						5													
						6													
						7		- Drilling becomes harder at 207'. Dry											
						8		basalt chips in cyclone											
						9		- softer drilling at 209'.											
						10													
						11		B BASALT: Gray-green, completely weathered,											
						12		chloritized basalt, appears to be residual											
						13		Rock thin, becomes highly vesicular.											
						14		Chloritized basalt at 213 - more competent											
						15		Rock, highly vesicular, Rock becomes											
						16		gray, highly vesicular basalt at 216'											
						17		competent basalt, some secondary chlorite,											
						18		Calcite, hard basalt.											
						19		Probably not interbed at 209'-216'.											
						20		Recovery: 56% RRD: 28%											
						21													
						22													
						23													
						24													
						25													
						26													
						27													
						28		Boring Terminated at 218' on 12/6/92.											
						29		Cav. encountered at 127 during drilling.											
						30													

Dames & Moore

LOCATION OF BORING <div style="text-align: center;"> </div>		JOB NO. 06702-006-111 CLIENT USATHAMA LOCATION Umatilla OK DRILLING METHOD: Becker Hammer Triple drill (sq: 12" 9" 6") Reverse Circ. SAMPLING METHOD: Cal. Split Sp. 3" x 18" 140" ext. hammer 30" drop WATER LEVEL TIME DATE CASING DEPTH		BORING NO. 4-21 SHEET 1 of 11 DRILLING START TIME 1600 FINISH TIME DATE 11/15/92 DATE			
DATUM <div style="text-align: center;"> </div>		SURFACE CONDITIONS: Flat, brush: Sand field (Sage Brush)					
SAMPLER TYPE	INCHES RECORDED	Time - BLOWS - GAGING	SAMPLE DEPTH	BLOWS/FT SAMPLER	GRAVITY WATER	DEPTH IN FEET	SOIL GRAPH
Grab	-	1605	-	-	0.0	2	SP
U	5" 5"	1615	10.0	50.5	0.0	10	GP
						15	
						20	

SP SAND: Brown (7.5YR 5/3), <5-10% fines, >90-95% f-m sand - angular quartz; basalt, same esp, felsic, micaceous, poorly graded, dry, flint sand. -cuttings-

- increase in rounded f-m gravel, basalt clasts.

GP GRAVEL: Grayish Brown (DYE 5/2), <5% fines, 5-10% f-c sand (As Above), pred. f-c gravels, basalt, rounded to subrounded, poorly graded, dry, v. dense.

GRAVEL: As Above -cuttings- dry

DRILLING CONTR. **Lay. e. ind.**

No. 162888

BY **Maya A. Ochsner**
DATE **11/15/92** CHK'D BY

DMS-1 (3) (REV. 11-90)

Dames & Moore

DRILLING CONTR Layne Inc.
No. 162889

BY Mark Oster
DATE 11/15/92 CHK'D BY
GSD-1 (2) (REV. 11-90)

LOCATION OF BORING										JOB NO. 06702-086-111		CLIENT USA THAMDA		LOCATION Una tilga or					
See page 1										DRILLING METHOD:				BORING NO. 4-21					
										See page 1				SHEET 2 of 11					
														SAMPLING METHOD:					
														DRILLING					
														WATER LEVEL				START TIME	
TIME				DATE		DATE													
CASING DEPTH				DATE		DATE													
DATUM										ELEVATION									
SAMPLER TYPE	INCHES RECORDED	TIME	DEPTH OF CUTTING	SAMPLE NO.	BLOWS/FT SAMPLER	DRILL NUMBER & ZONES	DEPTH IN FEET	SOIL GRAPH	SURFACE CONDITIONS:										
Cuttings	-	1:05	-	-	0.0	20	GP	SANDY GRAVEL: Grayish-Brown (10YR 5/2), 30% f-c Sand, 70% m-c gravels, poorly graded, dry, dense, occasional cobble size basalt clasts. Sand is angular, pale, felsic, quartz, ksp, basalt, m-c gravels are angular basalt fragments - cuttings -											
						1													
						2													
						3													
						4													
						5		- cuttings are as above - v. dry.											
						6													
						7													
						8													
						9													
						30	GP	SANDY GRAVEL: Grayish-Brown (10YR 5/2), 20% f-c Sand, < 5% fines, 75% c gravels, poorly graded, dry, dense to v. dense, Sand is pale quartz, basalt, felsic, malacaceous, gravels are angular, basalt fragments - fresh.											
U	6'	1:05	2/30	60'	0.0	1		End of day											
						2													
						3													
						4													
						5		- cuttings as above Hand drilling											
						6													
						7													
						8													
						9													
						40													

Dames & Moore

LOCATION OF BORING										JOB NO.		CLIENT		LOCATION	
										06702-086-111		USATKMA		Umatilla OK	
										DRILLING METHOD:				BORING NO.	
														421	
										SAMPLING METHOD:				SHEET	
														3 of 11	
														DRILLING	
										WATER LEVEL		START		FINISH	
										TIME		TIME		TIME	
										DATE		DATE		DATE	
										CASING DEPTH					
DATUM										ELEVATION					
SAMPLER TYPE	MOORE'S DRIVE	INCHES PER MINUTE	DEPTH OF CASING	SAMPLE NO	BLOWS/FT	NUMBER OF RINGS	DEPTH IN FEET	SOIL GRAPH	SURFACE CONDITIONS:						
V	5"	4"	1700	3	400	905"	40	GW	SANDY GRAVEL: GRAYISH BROWN (10YR 5/2), < 5% fines, 25% F-C Sand, 75% M-C gravels, well graded, dry, dense. Sand is angular, felsic. Pred quartz & basalt - some kspn. Gravels are subrounded basalt, occasional angular basalt fragments. Alluvium						
							1								
							2								
							3								
							4								
							45		- becoming more mafic						
							6								
							7								
							8								
							9								
							50	GW	SANDY GRAVEL: GRAYISH BROWN (10YR 5/2) < 5-10% fines, 35% F-C Sand, angular, pred basalt, mafic, 25% F-C gravels, angular & subrounded, basalt, clasts and fragments, well graded, dense. Alluvium						
V	12"	10"	0800	4	520	1196"	1								
							2								
							3								
							4								
							5	GW	- cuttings are pred. Sand & gravel highly mafic - pred basalt.						
							6								
							7								
							8								
							9								
							60								

See Page 1

See Page 1

DRILLING CONTR Layne G.W.
No. 162878

BY Mark A. Schaefer
DATE 11/15/92 CHK'D BY

980.1 (2) (REV. 11-90)

Dames & Moore

No. 162892
 DRILLING CONTR. Cape Fear

BY Mark Ochner
 DATE 11/16/92 CHK'D BY

LOCATION OF BORING										JOB NO.		CLIENT		LOCATION					
See Page 1										010202086-III		USA-THMA		UNAGILLG OK					
										DRILLING METHOD:				BORING NO.					
														4-21					
										SAMPLING METHOD: <u>See Page 1</u>				SHEET					
														4 of 11					
										DRILLING									
										WATER LEVEL		START		FINISH					
										TIME		TIME		TIME					
										DATE		DATE		DATE					
										CASING DEPTH									
DATUM										ELEVATION									
SAMPLER TYPE	INCHES ENTERED	INCHES RECOVERED	DEPTH OF CASING	SAMPLE NO	BLOWS/FT SAMPLER	NUMBER OF FEET	DEPTH IN FEET	SOIL GRAPH	SURFACE CONDITIONS:										
4	4	10	0830	5	600	9	0.0	GW	SAND GRAVEL: Gray (7.5R 6/10), 35% F-c Sand, angular to subrounded, mafic, pred-basalt, 105% F-m gravel, subrounded basalt, dry well gr. Sand increasing w/ depth - Cuttings becoming										
							1												
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							5												
							6												
							7												
							8												
							9												
4	18	15	0845	6	700	12	0.0	SP	GRAVELLY SAND: Gray (7.5R 5/10), < 5% fines, 25% angular to subrounded basalt gravel, 75% F-c Sand, angular to subrounded, poorly graded, dry, dense. increasing gravel w/ depth										
							1												
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							4												
							5												
							6	GW											
							7												
							8												
							9												
								80											

Dames & Moore

DRILLING CONTR. Wayne Env.

No. 162893

BY Mark Ochser
DATE 11/16/92 CHK'D BY

0.1 (2) (REV. 11-90)

LOCATION OF BORING										JOB NO.		CLIENT		LOCATION	
<div style="text-align: center; font-size: 2em;">See Page 1</div>										DRILLING METHOD:				BORING NO.	
														4-21	
										SAMPLING METHOD				SHEET	
														5 of 11	
										DRILLING					
										START TIME		FINISH TIME			
										DATE		DATE			
DATUM										WATER LEVEL		CASING DEPTH			
ELEVATION										TIME					
										DATE					
SAMPLER TYPE	INCHES DRIVEN	DEPTH OF CASING	SAMPLE NO.	BLOWS/FT SAMPLER	REMARKS	DEPTH IN FEET	SOIL GRAPH	SURFACE CONDITIONS:							
U	5"	0930	7	50-5"	0.0	80	GP	GRAVEL: GRAY (10YR 5/6), 25% fines, 10% F-m Sand, Pred. angular to subrounded basalt gravel, poorly graded, dense, dry							
						1									
						2									
						3									
						4									
						5									
						6		Gravel becomes rounded to well rounded							
						7									
						8									
						9									
						90	GP	GRAVEL: GRAY (10YR 5/6), 10% F-m Sand, angular basalt, Pred. rounded F-m basalt gravel, poorly graded, dry, occasional 1-2" pieces of highly vesicular basalt							
U	6"	1015	8	50-6"	0.0	1									
						2									
						3									
						4									
						5									
						6		- Drilling becomes V. HARD 4-6" cobbles in cuttings							
						7									
						8									
						9									
						10									

Dames & Moore

See Page 1										JOB NO. 06702-086-111		CLIENT USA THAMA		LOCATION Wahila OK			
										DRILLING METHOD:						BORING NO. 421	
										SAMPLING METHOD: See Page 1						SHEET 6 of 11	
										WATER LEVEL						DRILLING	
										TIME						START TIME	
DATE						FINISH TIME											
CASING DEPTH						DATE		DATE									

DATUM				ELEVATION						SURFACE CONDITIONS:	
SAMPLE TYPE	INCHES DRIVEN RECORDED	DEPTH OF CASING	SAMPLE NO.	BLOWS/FT SAMPLER	NUMBER OF FINES	DEPTH IN FEET	SOIL GRAPH				
Cuttings	1045	Grab	-	100	GP	SANDY GRAVEL: Gray (10YR 5/6) < 5% fines, 45% F-C angular Sand - Pred basalt, mafic, some 55% angular to subangular basalt gravels, poorly graded, dry, dense					
				1							
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				6							
				7							
				8							
				9							
Cuttings	1110	Grab	-	110	GP	GRAVEL: Gray (10YR 5/6) < 5% fines, < 10% F-C Sand, Pred. rounded to angular basalt, poorly graded, dry, dense.					
				1							
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				18							
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				20							

BY: Mark Johnson
 DATE: 11/16/92
 CHK'D BY:
 No. 162894
 DRILLING CONTR: Lloyd SWU

Dames & Moore

DRILLING CONTR Leape & Co.
No. 162895

BY Mark Adams
DATE 11/16/92 CHK'D BY
GSS-1 (3) (REV. 11-90)

LOCATION OF BORING								JOB NO.		CLIENT		LOCATION			
<div style="position: relative; height: 100px;"> See page 1 </div>								06702-000-111		USATAMA		MATHIA OR			
								DRILLING METHOD:						BORING NO.	
								See page 1						4-21	
														SHEET	
								SAMPLING METHOD:						7 of 11	
DRILLING						START		FINISH							
WATER LEVEL						TIME		TIME							
TIME						DATE		DATE							
DATE						DATE		DATE							
CASING DEPTH						DATE		DATE							
DATUM								ELEVATION							
SAMPLER TYPE	INCHES DRIVEN	INCHES RECORDED	DEPTH OF CASING	SAMPLE NO	BLOWS/FT SAMPLER	WATER-TO-RANGE	DEPTH IN FEET	SOIL GRAPH	SURFACE CONDITIONS:						
Cuttings			140	X	Grab	0.0	20	GP	<p>GRAVEL: Gray (10YR 5/2) little or no fines, pred subrounded to rounded basalt gravel, occasional angular fragments, dry, v. dense to hard, no spec collected due to v. hard drilling, poorly graded.</p> <p>- Cuttings become saturated at 123 lbs</p> <p>- Cuttings become finer w/depth.</p> <p>- Cuttings become coarse sand to fine gravel</p>						
							1								
							2								
							3								
							4								
							5								
							6								
							7								
							8								
							9								
U	10	15	1200	9	130	16/133	0.0	130	SP	<p>GRAVELLY SAND: Grayish Brown (10YR 5/2) <5% fines, 20-25% F-m angular basalt gravels, 75-90% F-C Sand, pred coarse angular, basaltic, highly mafic, saturated, dense.</p> <p>Cuttings become fine gravels. saturated</p> <p>GRAVEL: Gray to dk Gray (7.5YR 4/0), <5% fines, <10% sand, pred F-m rounded to subrounded basalt, saturated, dense, highly mafic</p>					
							1								
							2								
							3								
							4								
							5								
							6								
							7								
							8								
							9								
U			1220	10	135	14/119		135	GP						
							1								
							2								
							3								
							4								
							5								
							6								
							7								
							8								
							9								
								140							
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Dames & Moore

LOCATION OF BORING <div style="font-size: 2em; transform: rotate(-15deg); position: absolute; top: 100px; left: 100px;">See Page 1</div>					JOB NO. 06702 086-111		CLIENT USA THAMA		LOCATION Uwahilla OK			
					DRILLING METHOD: <div style="font-size: 1.5em; transform: rotate(-15deg); position: absolute; top: 10px; left: 10px;">See Page 1</div>						BORING NO. 4-21	
					SAMPLING METHOD:						SHEET 8 of 11	
					WATER LEVEL						DRILLING	
					TIME						START TIME	
DATE						DATE		FINISH TIME				
CASING DEPTH								DATE				

DATUM				ELEVATION				DEPTH IN FEET	SOIL GRAPH	SURFACE CONDITIONS:
SAMPLER TYPE	INCHES DRIVER RECORD	DEPTH OF CASING	SAMPLE NO	BLOWS/FT SAMPLE	NUMBER OF TURNS					
U	18/5	1245	10/140	17/137	0.0	140	GP		GRAVEL: Gray (7.5YR 4/0), < 5% fines, 5-10% m-c sand, subrounded basaltic, > 90% f-m gravels, subrounded basalt, slightly weathered, saturated, dense.	
						1				
						2				
						3				
U	18/0	1310	X	17/125	0.0	145	GP		NO RECOVERY - Cuttings indicate f-m gravels (basalt) Increasing fines w/ depth	
						6				
						7				
						8				
						9	SM/ML		SANDY SILT: Dk grayish brown (2.5Y 4/2), 60% fines, 40% v. fine to fine angular sand, felsic, saturated, glassy plastic, soft-med stiff, occasional fine basalt gravels.	
						1				
						2				
						3				
U	18/12	1320	11/150	16/110	0.0	150	B		Fragments of Lt Tan cemented ash (tuff) at 143' - Harder drilling at 154' - Refusal at 154.5' bgs w/ Becker rig Basalt: Dk Gray (7.5YR 4/0), slight to moderate weathering, vesicular, weathered horizontal fracturing, recovering chips from cyclone, dry.	
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See Page 1

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See Page 1

LOCATION OF BORING										JOB NO.		CLIENT		LOCATION					
See Page 1										06101-006-111		USATM & A		Unatilly or					
See Page 1										DRILLING METHOD:		BORING NO.		4-21					
See Page 1										SAMPLING METHOD:		SHEET		9 of 11					
See Page 1										WATER LEVEL		START		FINISH					
See Page 1										TIME		TIME		TIME					
See Page 1										DATE		DATE		DATE					
See Page 1										CASING DEPTH		DATE		DATE					
DATUM										ELEVATION									
SAMPLER TYPE	INCHES DEPTH	INCHES DEPTH	DEPTH OF CASING	SAMPLE NO	BLOWS/FT SAMPLER	NUMBER OF RINGS	DEPTH IN FEET	SOIL GRAPH	SURFACE CONDITIONS:										
							160		- Basalt chips discharging from cyclone.										
							1												
							2												
							3												
							4		BASALT: 1+ Gray (2.5Y 6/0), vesicular basalt, fine grained, occasional ca plug in mafic matrix, horizontal fracturing with some Fe staining at 167'										
							5		NO Gneiss, no pyrite, chlorite, calcite minerals.										
							6		- Similar to top flow encountered at 4-19.										
							7		Compacted Rock										
							8		Recryst = 100%										
							9		ROD = 33%										
							10		- Set 8" casing from surface to 167' - cemented in place.										
							11		- Some H ₂ O return at 168-169'										
							12		- Cuttings are fresh basalt chips - some water										
							13												
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Dames & Moore

DRILLING CONTR Laurel Inc.
No 198199

BY Mark Ockner
DATE 11/19/92 CHK DRY

QAD 1 (2) (REV 91-00)

LOCATION OF BORING										JOB NO. 0606-086-11		CLIENT USA THAM A		LOCATION Umatilla OR					
See Page 1										DRILLING METHOD:				BORING NO. 4-21					
										See Page 1				SHEET 10 of 11					
														SAMPLING METHOD:					
														DRILLING					
														WATER LEVEL				START TIME	
TIME				DATE		DATE													
CASING DEPTH				DATE		DATE													
DATUM										ELEVATION									
SAMPLER TYPE	INCHES ENTERED	DEPTH OF CASING	SAMPLE NO	BLOWS/T SAMPLER	NUMBER OF RINGS	DEPTH IN FEET	SOIL CHART	SURFACE CONDITIONS											
						180	B	BASALT: Lt. Gray (2.5% G10), fracture. basalt, Aphanitic, becomes fractured & weathered at 182-183', occasional vertical fracturing, Significant Chlorite filling @ 184', blue-green color. dry.											
						1													
						2													
						3													
						4		Basalt is fresh at 180-181. Becomes more fractured with depth.											
						5		Recovery: 100% RQD = 66%											
						6		- V. hard Drilling at 185' - Fresh basalt											
						7		Chips discharging											
						8		- Basalt dust (blue gray) V. dry											
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						19		- Tool drop from 189-191' - Fracture zone?											
						20													
						21		- Drilling Becomes hard again at 191'											
						22													
						23													
						24													
						25	B	- V. hard: dry - Fresh basalt chips as above.											
						26													
						27													
						28													
						29													
						30		- Drilling becomes softer at 191'											
						31		will core at 200'											
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LOCATION OF BORING										JOB NO.		CLIENT		LOCATION	
										06702-006-11		USASTHANA		CUMATILG OR	
										DRILLING METHOD:				BORING NO.	
														4-21	
										SAMPLING METHOD:				SHEET	
										See Page 1				11 of 11	
														DRILLING	
										WATER LEVEL				START	
														TIME	
										TIME				1230	
										DATE				DATE	
										CASING DEPTH				11/19/72	
DATUM										ELEVATION					
SAMPLER TYPE	INCHES RECORDED	DEPTH OF CASING	SAMPLE NO.	BLOWS/FT SAMPLER	NUMBER OF HITS	DEPTH IN FEET	SOIL CLASS	SURFACE CONDITIONS							
						200	B	BASALT: Green Gray (56 G/L), Poor Recovery, highly weathered, chloritized zones, Rock was obviously rolled around in Core Barrel, becomes vesicular at 202'. No Recovery from 202-208'. dry, sand Interbed?							
						1		Recovery: 25%							
						2		RDP: 8%							
						3									
						4									
						5									
						6									
						7									
						208		- Clean hole w/ 5 1/2" hammer to 210'. Cuttings are greenish Basalt (Chlorite)							
						9									
						210	B	BASALT: Green Gray (56 G/L), highly weathered, vesicular basalt, chloritized to 213'. Becomes Lt Gray (25 G/L) aphanitic basalt, fresh, minor vesicles filled with secondary calcite - competent Rock, no Recovery from 214-215'							
						1		Recovery: 80%							
						2		RDP = 33%							
						3									
						4									
						5									
						6		Coring terminated at 215'. Ream hole to 215'. 11/19/72							
						7		G.W. encountered at 123 during drilling, shallow aquifer							
						8									
						9									
						0									

See Page 1

DRILLING CONTR. Cape End.

No. 161961

BY Mark Ochsner

DATE 11/19/72 CHK'D BY

000.1 (3) (REV 11-00)

Dames & Moore

DRILLING CONTR Wayne Enrl.

No 198192

BY Mark A. Ochsner

DATE 12/3/92 CHK'D BY

935 I.131, REV 11-90

LOCATION OF BORING										JOB NO.		CLIENT		LOCATION	
										06702006-111		USATAMA		Umatilla OK	
DRILLING METHOD: <u>Becker Hammer</u> <u>Reverse Circulation</u> <u>Triple and Casing: 12"-9'6"</u>										BORING NO.		4-22			
SAMPLING METHOD: <u>Calif Split Stem 3"x18"</u> <u>140' ext. hammer 30' Drop</u>										SHEET		1 of 6			
WATER LEVEL TIME DATE										DRILLING		START FINISH			
CASING DEPTH										TIME		TIME			
DATE										DATE		DATE			
DATUM ELEVATION										12/1/92		DATE			
SAMPLER TYPE	INCHES DRIVER DISCOVERED	DEPTH OF CASING	SAMPLE NO	BLOWS/FT SAMPLER	NUMBER OF RINGS	DEPTH IN FEET	SOIL GRAPH	SURFACE CONDITIONS:							
						0		Relatively flat, sand: brush field							
						1									
						2									
						3									
						4									
						5	SP	SAND - angular, poorly graded, micaceous, - clt fines - Pleist. sands							
						6									
						7									
						8									
						9									
						10	SP	SAND: Brown (7.5% 5/3), 5-10% fines, 79.0% fine sand, angular quartz, felsic, poorly graded, dump, medium dense, micaceous Pleist. sand							
U	18	1055	10.0	19/10	0.0	1									
						2									
						3									
						4									
						5									
						6									
						7									
						8		- increase in silt							
						9									
						20	SM								

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LOCATION OF BORING										JOB NO.		CLIENT		LOCATION					
See Page 1										0602086		USATHAMA		Vineville OK					
DRILLING METHOD:										DRILLING NO.		4-22		SHEET					
SAMPLING METHOD:										See Page 1		206		DRILLING					
WATER LEVEL										START		FINISH		TIME					
TIME										DATE		DATE		DATE					
CASING DEPTH										DATE		DATE		DATE					
DATUM										ELEVATION									
SAMPLER TYPE	INCHES DRIVEN	INCHES PENETRATED	INCHES DEPTH	INCHES CORING	SAMPLE NO.	BLOWS/FT	SAMPLER	DEPTH IN FEET	SOIL GRAPH	SURFACE CONDITIONS									
4	18	11	15	2	19	11	0.0	20	SM	SILTY SAND: Brown (7.5YR 5/2), 25-30% fines, 70-75% v. fine to fine sand, poorly graded, non-plastic, damp, med. dense. Sand is angular quartz, feldspar; some basalt, felsic, micaceous. Plast. Sand									
								1											
								2											
								3											
								4											
								5											
								6											
								7		- cuttings became saturated at 27.0'									
								8											
								9											
								10											
								11											
								12											
								13											
								14											
								15											
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								40											

DRILLING CONTR Layne Engr.

BY Mark A. Schaner

DATE 12/3/92 CHK'D BY

Dames & Moore

No. 161964

BY: Mark Oelsner

DATE: 12/4/72 CHK'D BY:

800.1 (2) (REV 11-60)

LOCATION OF BORING										JOB NO.		CLIENT		LOCATION							
See Page 1										0610-006		USATHAM A		Umatilla OK							
										DRILLING METHOD:										BORING NO.	
										Air Rotary 55'										4-22	
										NACORE										SHEET	
										306											
SAMPLING METHOD:										DRILLING											
NWL Core barrel 2.985" Dia. x 6'										START		FINISH									
TIME										TIME		TIME									
DATE										DATE		DATE									
CASING DEPTH																					
DATUM										ELEVATION		SURFACE CONDITIONS									
SAMPLE TYPE	TESTS	RECORDS	TESTS	RECORDS	TESTS	RECORDS	TESTS	RECORDS	TESTS	RECORDS	IN FEET	SOIL GRAPH									
U	18	12	15	4	10	14	10	0.0	40	ML			SILT: Lt Brown (10% red) to olive gray (5% red), 25-10% v. fine sand, thin 0.5-1.0 mm color reddish. Alternates Lt Brown to olive gray, well compacted. Pieces of silt, appears to be low energy lake deposit. 'clayey', moist, not saturated, very stiff.								
									1												
									2												
									3												
									4												
									5												
									6				Cuttings - silt, dry-moist, micaceous								
									7												
									8												
									9												
									50	ML			SANDY SILT: Brown (7.5% red), 25-30% v. fine fine sand, angular, quartz, felsic, 70-75% fines, non-plastic, occasional Fe staining, well compacted silt, some mica present.								
U	18	12	15	5	10	14	10	0.0	1												
									2												
									3												
									4												
									5												
									56	B			Casing refusal at 56.0' w/ Becker Hammer move-in air rotary rig								
									7				BASALT: Gray (7.5% red) (Core run 55-57.5') highly weathered, highly fractured basalt, vesicular, horizontal fracturing, some Fe staining at fractures, no apparent secondary minerals. R.O.D. = 99% Recovery = 100%								
									8												
									9												
									60												

Dames & Moore

DRILLING CONTR Laquey Tech
No. 161965

BY Mark Ochsen
DATE 12/4/92 CHK'D BY
088.1 (2) (REV 11-90)

LOCATION OF BORING										JOB NO. 06702-086-111		CLIENT KATHARNA		LOCATION Vmatilla OK					
<div style="position: absolute; top: 100px; left: 200px; font-size: 2em; transform: rotate(-15deg);">See Page 1</div>										DRILLING METHOD: Air Rotary Th too		BORING NO. 4-22							
										SAMPLING METHOD: 1 1/2" Core Barrel 2-985" x 10"		SHEET 4 of 6							
										WATER LEVEL		START TIME							
										TIME		FINISH TIME							
DATE		DATE		DATE		DATE													
CASING DEPTH																			
DATUM										ELEVATION									
SAMPLER TYPE	INCHES DEPTH	INCHES DEPTH	DEPTH OF CASING	SAMPLE NO	ULTIMATE SAMPLE	NUMBER OF RINGS	DEPTH IN FEET	SOIL GRAPH	SURFACE CONDITIONS										
							60	B	- Cuttings are dr basalt chips										
							1												
							2												
							3												
							4												
							5												
							6												
							7		- Bottom of B" (Cg) completed at 67' bgs. to Surface.										
							8	B	- Drilling becomes hard at 67' - Dry blue gray dust; basalt chips in cyclone										
							9		Drilling Rates: (5 1/2") 12 min/ft.										
							70												
							1												
							2												
							3												
							4												
							75	B	BASALT: Lt Gray (7.5YR 6/0), highly fractured, aphanitic basalt, becomes less fractured at 77-84.5'. Rock becomes competent basalt, no visible secondary minerals, slightly vesicular, dry, hard.										
							6		Recovery: 100% RQD: 79%										
							7												
							8												
							9												
							80												

Core run #2
75-84.5'

Dames & Moore

No. 161966 DRILLING CONTR Layne and

BY Mark Ochsmid DATE 12/01/92 CHK'D BY

LOCATION OF BORING										JOB NO.	CLIENT	LOCATION	
See page 1										06028-11	USAID/WWA	Waukegan, IL	
										DRILLING METHOD:		BORING NO.	
										Air Rotary TH 60		4-22	
										SAMPLING METHOD:		SHEET	
										NW core barrel		506	
										2.905" x 10'		DRILLING	
										WATER LEVEL		START TIME	FINISH TIME
										TIME		DATE	DATE
										DATE			
										CASING DEPTH			

DATUM	ELEVATION	SAMPLER TYPE	INCHES DRIVEN	INCHES RECORDED	DEPTH OF CASING	SAMPLE NO.	BLOWS/FT SAMPLER	NUMBER OF RINGS	DEPTH IN FEET	SCH. GRADE	SURFACE CONDITIONS
	80									B	Continue core run #2 to 89.5'
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	3										
	4										
	5										
	6										
	7										
	8										
	9										
	90										
	1										
	2										
	3										
	4										
	5										
	6										
	7										
	8										
	9										
	100										

Dames & Moore

LOCATION OF BORING				JOB NO.		CLIENT		LOCATION			
See Page 1				06102-086-111		USATHAMA		Umatilla OK			
				DRILLING METHOD:						BORING NO.	
				See Page 1						4-22	
										SHEET	
										606	
SAMPLING METHOD:				WATER LEVEL		START		FINISH			
See Page 1				TIME		TIME		1200			
				DATE		DATE		12/9/92			
				CASING DEPTH							
DATUM				ELEVATION							
SAMPLER TYPE	INCHES	DEPTH OF CASING	SAMPLE NO.	USCONS/FT	NUMBER OF	INCHES	SOIL	SURFACE CONDITIONS			
TYPE	RECORDED	DEPTH	DEPTH	SAMPLER	WINGS	IN FEET	GRAPH	See Page 1			
						100	B	Basalt: Dk Blue-green, highly weathered, chloritized basalt - upper 2' sharp contact at 102' to 1' brown (10yr 8/3) silt, ash, sandy gravel, probably Selah Interbedded material? not saturated, moist RQD = 17% Recovery = 80%			
						101	GM	Probable Selah Interbed 102-109'			
						102					
						103					
						104					
						105					
						106					
						107		Drilled w/ 5 1/2" hammer: harder drilling at 109'. Blue-gray basalt chips and dust in cuttings, Dry.			
						108					
						109	B				
						110					
						111					
						112		- Continued hand drilling at 112'. Basalt chips in cyclone - Fresh blue-gray basalt. Dry.			
						113					
						114	B				
						115		Basalt: Gray (7.5% - 6%), aphanitic basalt, vesicular, some secondary olivine in vesicles, larger vesicles with lt blue staining on rim, could be Chlorite, competent Rock from 109'. Dry.			
						116		RQD = 43% Recovery = 100%			
						117					
						118					
						119		Boring Terminated at 119' on 12/9/92.			
						120		G.W. encountered at 27.0' during drilling.			

Dames & Moore

LOCATION OF BORING		JOB NO.	CLIENT	LOCATION
AREA VI		06737-08	USATHAMA	OR
		DRILLING METHOD: Becker hammer		BORING NO.
		Dual wall casing reverse		MW-4-23
		Circulation 9"OD 6"ID		SHEET
		SAMPLING METHOD: Calif. mod.		1 of 16
		Split spoon 3"OD x 18" 140#		DRILLING
		30" drop external hammer		START TIME
		WATER LEVEL		FINISH TIME
		TIME		0745 1700
		DATE		DATE DATE
		CASING DEPTH		11/15/92 11/15/92

DATE	INCHES DRIVEN	DEPTH OF CASING	SAMPLE DEPTH	BLOWS/FT SAMPLER	NUMBER OF WINGS	DEPTH IN FEET	SOIL GRAPH	SURFACE CONDITIONS
								Flat gravelly sandy Field, sage brush.
0800						0.0	SP	SAND Reddish brown (5 YR 4/3) 90-95% fine - med gr. poorly graded, subround - ind. basaltic & gtz. sand, ciccas gravel, fine - med grained, subround 2-10% silt dry loose. No enter
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DRILLING CONTR. Gayne

No. 162901

BY Chas. Cooley

CHK'D BY

DATE

DS 1 (3) (REV 11-90)

Dames & Moore

LOCATION OF BORING 				JOB NO. 		CLIENT 		LOCATION 			
				DRILLING METHOD: See Page 1				BORING NO. 4-23			
See Page 1				SAMPLING METHOD: 				SHEET 2 of 6			
				WATER LEVEL 				DRILLING 		START TIME 	
DATUM 				CUM ELEVATION 				TIME 		DATE 	
								Casing Depth 		DATE 	

SAMPLER TYPE	INCHES DOWN IN CLOGGED	DEPTH OF CASING	SAMPLE NO.	BLOWS/FT SAMPLED	NUMBER OF ROD PISTONS	DEPTH IN FEET	SOIL GRAPH	SURFACE CONDITIONS:
	6"		1514	10.0	20	GP		SANDY GRAVEL Brown 2.5YR 5/2 65-70% med-coarse subrounded poorly graded gravel 25-30% med-fine gr. Sand 40% Silt dry-moist, loose, w/ basalt cobbles up to 5" dia, qtzite, wtd feldspar. Sand is 60% Basaltic, 40% Qtzite.
					1			
					2			
					3			
					4			
					5			A/A
					6			Abundant Basalt cobbles up to 4" dia
					7			
					8			
					9			
935	18" 12"		1114	0.0	30	GP		SANDY GRAVEL Brown (2.5YR 4/2) 70-80% med-coarse gravel, 15-25% Sand (AA) 40% Silt, dry loose wtd feldspar qtzite. w/ cobbles, fractured & subrounded
					1			
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No.162902

BY DATE CHK'D BY

Dames & Moore

LOCATION OF BORING		JOB NO.	CLIENT	LOCATION
		DRILLING METHOD:		BORING NO.
		SEE		4-23
		SAMPLING METHOD: PAGE		SHEET
		1		3 of 10
		DRILLING		
WATER LEVEL		START	FINISH	
TIME		TIME	TIME	
DATE		DATE	DATE	
CASING DEPTH				

DATUM	CUM. ELEVATION	SAMPLER TYPE	INCHES DRIVEN	INCHES RECORDED	DEPTH OF CASING	SAMPLE NO.	BLOWS/FT	SAMPLER	NUMBER OF THINGS	DEPTH IN FEET	SOIL GRAPH	SURFACE CONDITIONS
		85514	4"			11/19/	50	C.O.	0.0	40		Recovered only basalt fragments - will log Ctg's
										1		
										2		
										3		
										4		
										4.5		
										5		
										6		
										7		
										8		
										9		
										10		
		922	Ctg's						0.0	50		Abundant basalt cobble frags
										51		
										52		
										53		
										54		
										55		
										56		
										57		
										58		
										59		
										60		

No. 162903

928 1 (3) (REV 11-00) BY _____ DATE _____ CHK'D BY _____

Dames & Moore

No. 162846

DRILLING CONTR

938.1 (3) (REV 11-00)

LOCATION OF BORING										JOB NO.		CLIENT		LOCATION			
										DRILLING METHOD: <div style="font-size: 1.2em; font-family: cursive;">See Page 1</div>				BORING NO. <div style="font-size: 1.2em; font-family: cursive;">4-23</div>			
										SAMPLING METHOD:				SHEET <div style="font-size: 1.2em; font-family: cursive;">4</div> of <div style="font-size: 1.2em; font-family: cursive;">10</div>			
										WATER LEVEL				START TIME		FINISH TIME	
										TIME				DATE		DATE	
DATE										C/M ELEVATION		CASING DEPTH		SURFACE CONDITIONS:			
SAMPLER TYPE	INCHES DRIVEN RECORDED	DEPTH OF CASING	SAMPLE DEPTH	BLOWS/FT SAMPLER	NUMBER OF HITS	DEPTH IN FEET	SOIL CLASS										
CTGS					0.0	60	GW	<div style="font-family: cursive; font-size: 0.9em;"> SANDY GRAVEL Dark brown (7.5 YR 4/2) 70-80% Basaltic med-coarse subrounded-rounded, well graded Gravel 20-25% Fine-coarse subrounded-subangular, well graded Qtz & basalt Sand <10% Silty Quartzite present weathered Feldspar Abundant Basalt cobbles & boulder frags. slightly moist. </div>									
						1											
						2											
						3											
						4											
CTGS					0.0	5		<div style="font-family: cursive; font-size: 0.9em;"> A/A </div>									
						6											
						7											
						8											
						9											
CTGS					0.0	70	GW	<div style="font-family: cursive; font-size: 0.9em;"> SANDY GRAVEL A/A </div>									
						1											
						2											
						3											
						4											
CTGS					0.0	5	GW	<div style="font-family: cursive; font-size: 0.9em;"> SANDY GRAVEL A/A NO REC. </div>									
						6											
						7											
						8											
						9											
						79											
						0											

Dames & Moore

No. 162843

DRILLING CONTR

BY DATE

CHK'D BY

LOCATION OF BORING										JOB NO.		CLIENT		LOCATION			
										DRILLING METHOD:				BORING NO.			
										See page 1				4-23			
														SHEET			
														506			
										SAMPLING METHOD:				DRILLING			
														START		FINISH	
														TIME		TIME	
														DATE		DATE	
WATER LEVEL										CASING DEPTH		DATE		DATE			
TIME																	
DATE																	
ELEVATION																	
DATUM																	
SAMPLER TYPE	INCHES DRIVEN INCHES RECORDED	DEPTH OF CASING	SAMPLE NO. SAMPLE DEPTH	BLOWS/FT SAMPLER	NUMBER OF HITS	DEPTH IN FEET	SOIL GRAPH	SURFACE CONDITIONS									
CTGS					0.080	1	GW	SANDY GRAVEL (75% VR 30%) Very Dark Gray 70-80% Fine- Coarse, subrounded-subangular well graded, Basaltic Gravel 20-25% Fine-Coarse subrounded-subangular well graded Sand (60% basaltic 40% Quartzitic) <10% Silt with Abundant Basaltic cobbles & fragmented boulder fragments moist no odor									
						2											
						3											
						4											
CTGS					0.0	5		SANDY GRAVEL A/A									
						6											
						7											
						8											
CTGS					0.090	1		SANDY GRAVEL A/A									
						2											
						3											
						4											
CTGS					0.0	5		SANDY GRAVEL A/A									
						6											
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Dames & Moore

LOCATION OF BORING										JOB NO.		CLIENT		LOCATION	
										DRILLING METHOD:				BORING NO.	
										SAMPLING METHOD:				SHEET	
														DRILLING	
										WATER LEVEL				START TIME	
										TIME				FINISH TIME	
										DATE				DATE	
										CASING DEPTH					
DATUM										ELEVATION					
TIME	INCHES DRIVEN RECORDED	DEPTH OF CASING	SAMPLE DEPTH	GEOLGIST SAMPLED	OVM INTERVAL	DEPTH IN FEET	SOIL GRAPH	SURFACE CONDITIONS:							
CEGS				0.0		100		SANDY GRAVEL moist A/A							
						1									
						2									
						3									
						4									
CEGS				0.0		5		becoming moister							
						6									
						7									
						108		Wtr @ 108'							
						9									
CEGS				0.0		0		Dried to 110, pulled csg							
						11		back 2' & let sit.							
						2		Boring terminated @ 110' on 11/15/92.							
						3		GWL encountered @ 105' during drilling							
						4									
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						0									

Dames & Moore

DRILLING CONTR LYMR

No. 162880

Upper Corral

LOCATION OF BORING				JOB NO.		CLIENT		LOCATION			
				06732-086		USATHAMA		ORUMU 11a			
				DRILLING METHOD: <u>Decker Hammer</u>				BORING NO. <u>NW-4-24</u>			
				Dual wall casing reverse circulation, 9"OD, 6"ID				SHEET <u>1 of 6</u>			
				SAMPLING METHOD: <u>Calif Mod split</u>				DRILLING			
3' spoon 3"OD x 18" 140#				30" drop external hammer				START TIME			
WATER LEVEL 101.8 101.8 101.6 101.6				TIME 11:45 13:02 13:30 14:00				10:10 13:00			
DATE 11/14/92 11/14 11/14 11/14				DATE 11/14/92 11/14 11/14 11/14				DATE			
CASING DEPTH 110'				SURFACE CONDITIONS: <u>Gravelly, Sandy Field</u>							
TIME	INCHES DRIVEN	DEPTH OF CASING	SAMPLE NO.	REMARKS	DEPTH IN FEET	SOIL CLASS					
					0.0	SP	SAND Reddish Brown (SYR 413) 90-95% fine-med gr, poorly graded, subround-rnd, basaltic & gls sand, occas. gravel (fine-med gr, subrounded) <10% silt dry loose, no odor				
					2	GM	SILTY SANDY GRAVEL (7.5YR 5/2) 50-55% fine to med gravel, 2.5-30% med. to coarse sand, subrounded-subangular, poorly-med graded, gravel is rounded-angular. Silt is nonplastic, loose, dry-moist				
					10.25	GM	w/ Basalt Cobble up to 5" Black Massize.				
					10.25	GM	SILTY SANDY GRAVEL (7.5Y 5/2) Brown 60-70% med-coarse gr gravel, 10% silt, 2.5-30% fine gr. sand, poorly graded. Gravel is subrounded, basaltic. Sand is subrounded, rounded, silt is non plastic, dry loose				
					10.25	GM	SILTY SANDY GRAVEL A/A w/ <10% fine basalt cobbles (7.0%) angular, fractured, some subrounded, dry loose.				
					10.25	GM	A/A w/ basalt cobbles.				

Dames & Moore

LOCATION OF BORING				JOB NO.		CLIENT		LOCATION	
<div style="text-align: center; font-size: 2em; font-family: cursive;">See Page 1</div>				DRILLING METHOD:				BORING NO.	
								4-24	
				SAMPLING METHOD:				SHEET	
				See Page 1				2 of 6	
				WATER LEVEL				DRILLING	
				TIME				START TIME	
				DATE				DATE	
DATUM				ELEVATION				CASING DEPTH	
TIME	INCHES RECORDED	INCHES DRILL	DEPTH OF CASING	SAMPLE DEPTH	DI (CM) / IN (INCH)	QUM INFORMATION	DEPTH IN FEET	SOIL CLASS	SURFACE CONDITIONS
1943	2"	2"	2"	2"	30	0.0	20	GP	SANDY GRAVEL Brown (7.5YR 5/4) 65-70% Subrounded, med-coarse gravel, 28-30% fine grained, subrounded, poorly graded sand, <10% silt, non plastic, dry loose.
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Dames & Moore

DRILLING CONTR

No. 162880

BY _____ DATE _____
CHK'D BY _____

800 1 (3) (REV 11 80)

LOCATION OF BORING										JOB NO.		CLIENT		LOCATION	
<p>See Page 1</p>										DRILLING METHOD:				BORING NO.	
														4-24	
														SHEET	
										SAMPLING METHOD:				3 of 6	
										See Page 1				DRILLING	
WATER LEVEL										START TIME		FINISH TIME			
TIME										DATE		DATE			
DATE										CASING DEPTH					
DATUM										ELEVATION					
TIME	INCHES DOWN RECORDED	DEPTH OF CASING	SAMPLE NO.	BLOWS/F SAMPLE	QUM NUMBER	DEPTH IN FEET	SOIL GRAPH	SURFACE CONDITIONS							
11:10	0				0.0	40	GW	SANDY GRAVEL Dark brown (7.5 YR 4/2) 70-80% Basalt gravel & cobbles. Cobbles are highly fractured. Coarse-med grained gravel. 15-25% poorly graded subrounded, predominately basalt w/ qtz, fine-med grained sand. 12-10% S.S.							
11:20	0				0.0	4		A/A							
11:30	cuttings				0.0	50	GW	SANDY GRAVEL A/A @ 40' Some wtd quartzite, frags of cemented qtz basalt S.S.							
11:40	cuttings				0.0	42		A/A							

LOCATION OF BORING								JOB NO.	CLIENT	LOCATION
								DRILLING METHOD:		BORING NO. 4-24
										SHEET 406
								SAMPLING METHOD: <i>See Page 1</i>		DRILLING
								WATER LEVEL	START TIME	FINISH TIME
								TIME		
								DATE	DATE	DATE
								CASING DEPTH		
DATUM	ELEVATION	SURFACE CONDITIONS:								
<i>See Page 1</i>										
1155	8.0	G0	<i>A/A @ 50'</i>							
1150		1								
		2								
		3								
		4								
1150	0.0	5	<i>GW SANDY GRAVEL A/A @ 60' moist</i>							
		6								
		7								
		8								
		9								
1155	0.0	70								
		1								
		2								
		3								
		4								
1210	0.0	5	<i>Sandy Gravel, As Above A/A</i>							
		6								
		7								
		8								
		9								
		0								

Dames & Moore

DRILLING CONTR

No. 162880

BY DATE CHK'D BY

200 1 131 (REV 11 00)

LOCATION OF BORING										JOB NO.		CLIENT		LOCATION	
<p>See Page 1</p>										DRILLING METHOD:				BORING NO.	
														4-24	
														SHEET	
										SAMPLING METHOD:				5 of 6	
										See Page 1				DRILLING	
										WATER LEVEL		START TIME		FINISH TIME	
										TIME		DATE		DATE	
										DATE					
										CASING DEPTH					
DATUM										ELEVATION					
TIME	INCHES DOWN RECORDED	INCHES DOWN CASING	SAMPLE DEPTH	DIAMETER SAMPLER	OVM INCHES	DEPTH IN FEET	SOIL CLASS	SURFACE CONDITIONS							
12:20	1755				0.0	8		SANDY GRAVEL 7.5 YR 3/0 Vel. v Dark Gray 70-75% med-coarse gravel, med-mal graded subangular to subrounded gravel, 20-25% med-coarse subangular angular sand (60% basaltic, 40% Q12) 2-10% silt, moist loose. w/ fractured basalt cobbles.							
	1755				0.0	5		A/A							
11:30	1755				0.090	1	GW	Basalt Cobble fragments not as numerous.							
	1755				0.0	5	GN	A/A @ 80' numerous Cobble and/or boulder frags. Harder Drilling below 95'							
	1755					8	GW	A/A. Basalt frags contain Chlorite. Metamorphic Metamorphics (Gneiss) present.							

Dames & Moore

LOCATION OF BORING										JOB NO.		CLIENT		LOCATION	
See Page 1										DRILLING METHOD:				BORING NO.	
														4-24	
														SHEET	
										SAMPLING METHOD: See Page 1				6 of 6	
														DRILLING	
										WATER LEVEL		START TIME		FINISH TIME	
										TIME		DATE		DATE	
										DATE					
CASING DEPTH															
DATUM										ELEVATION					
TIME	INCHES DOWN	FEET DOWN	DEPTH OF CASING	SAMPLE NO.	INCHES DOWN	FEET DOWN	OVM	INCHES DOWN	FEET DOWN	SURFACE CONDITIONS					
12:45	0				50.0	6.0				SANDY GRAVEL Very Dark Gray 17.5YR 3/0. 70-75% med. coarse well graded gravel, subrounded-reounded, 20-25% well graded med. coarse grained, subrounded-subang. 60% Basaltic 40% Quarzitic Sand, <10% Silt dx. no. cder. moist, SANDY GRAVEL A/A					
12:50	6					0.0				ICS drilling a bit easier,					
										107 Free Water					
										SANDY GRAVEL Very Dark Gray 7.5YR 3/0 A/A well graded gravel well rounded sand.					
										Let sit 1 hr.					
										4.2' Stick up					
										106 103.8 13:40					
										4.2 4.2 101.6					
										101.8 WLE 13:02					
										Hole bottom 107.6 @ 13:30 107.6					
										105.8 @ 14:00 101.8 3.8 6.0					
										@ 13:02 @ 13:40					
										Boring terminated @ 113.5 m 11/14/02					
										Gw encountered at 107.6 during drilling.					

DRILLING CONTR

No. 162880

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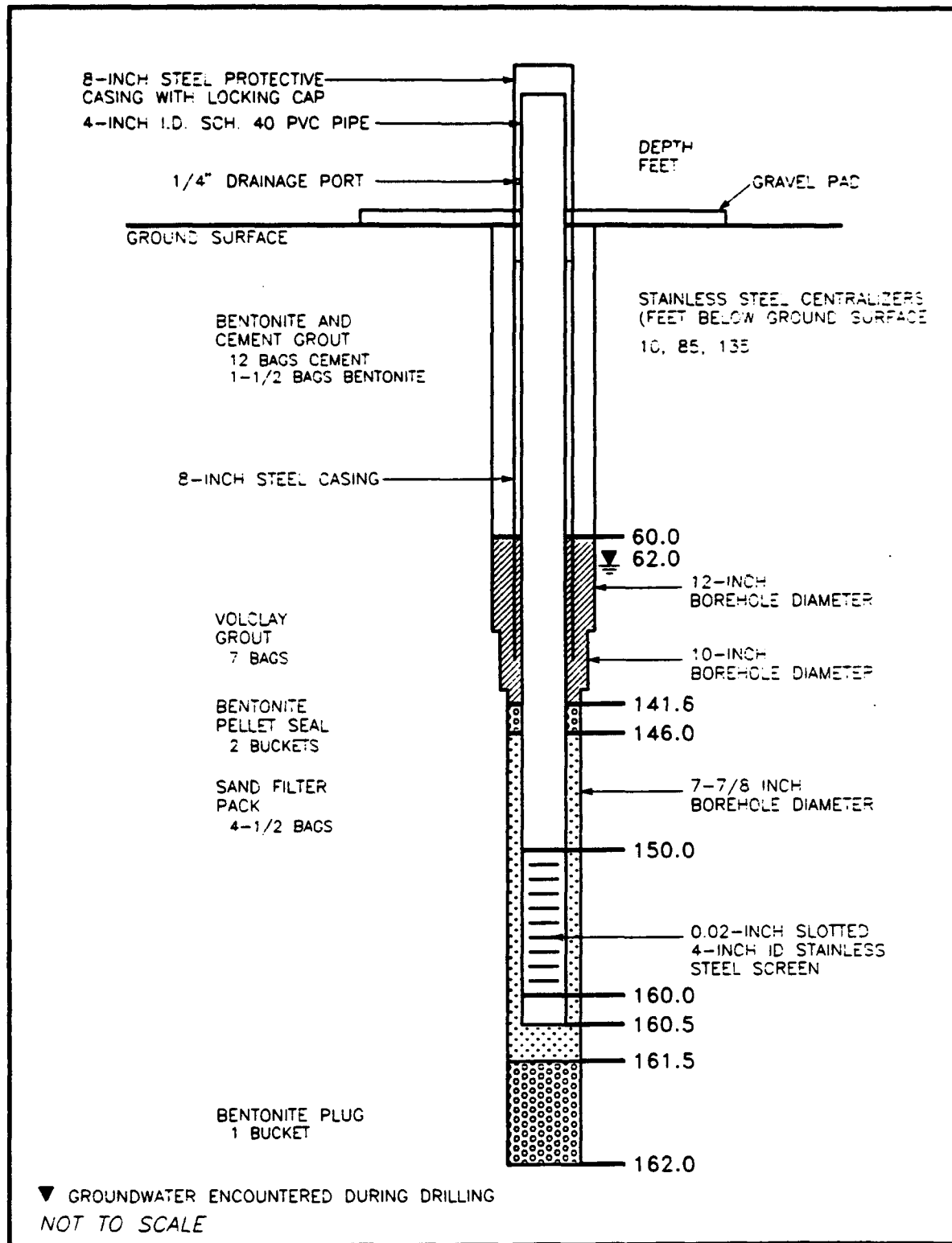
DATE

930 5 (3) (REV 11-00)

APPENDIX B
Well Construction Diagrams

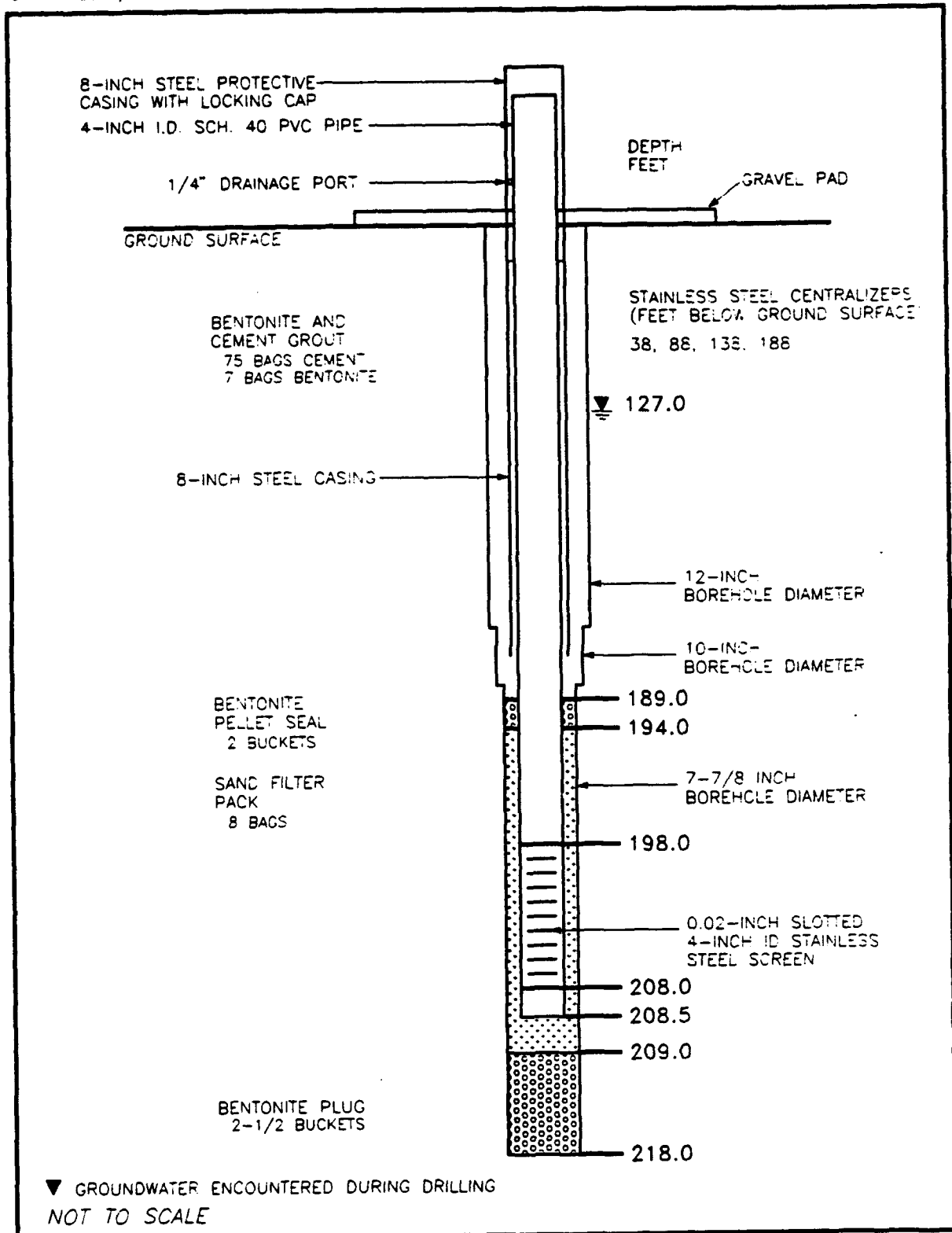
Well Installation Diagram
Explosive Washout Lagoons
Supplementary Remedial Investigation
UMATILLA, OREGON

Location: 4-19
 Installation Date: 11/17/92
 Surface Elevation: 557.80 Feet MSL
 Top of PVC Elevation: 559.59 Feet MSL



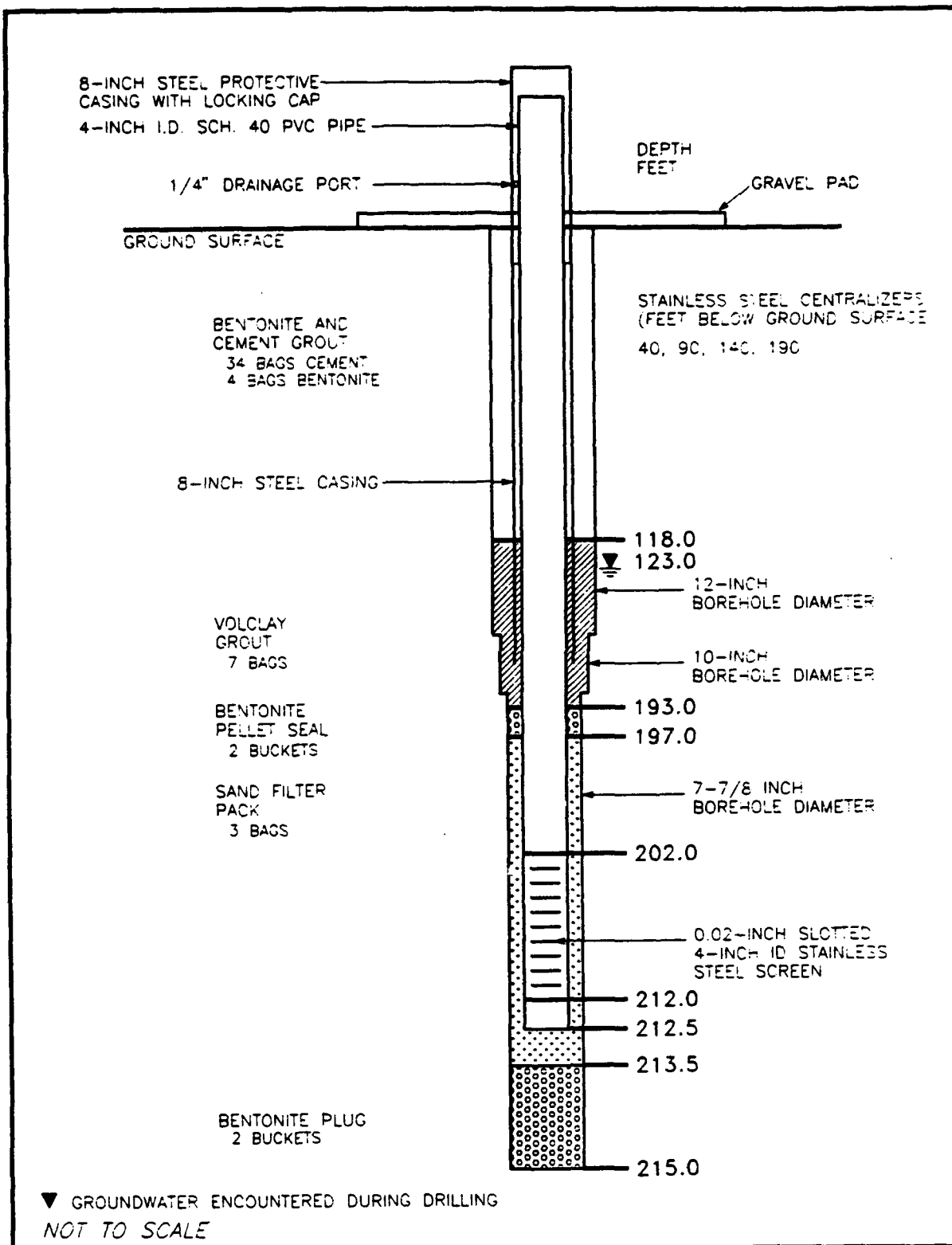
Well Installation Diagram
Explosive Washout Lagoons
Supplementary Remedial Investigation
UMATILLA, OREGON

Location: 4-20
Installation Date: 12/09/92
Surface Elevation: 616.40 Feet MSL
Top of PVC Elevation: 617.45 Feet MSL



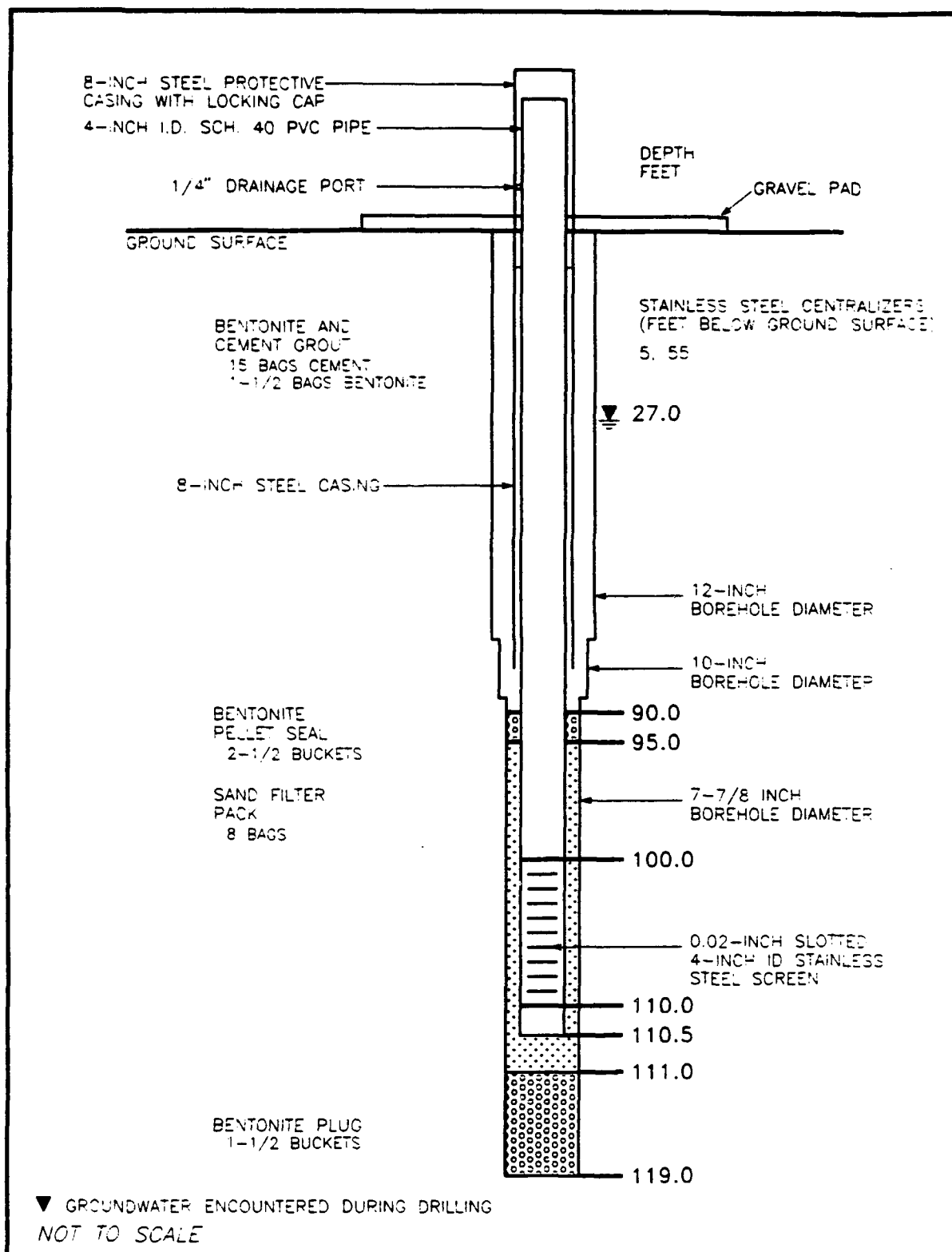
Well Installation Diagram
Explosive Washout Lagoons
Supplementary Remedial Investigation
UMATILLA, OREGON

Location: 4-21
Installation Date: 11/21/92
Surface Elevation: 614.60 Feet MSL
Top of PVC Elevation: 616.57 Feet MSL



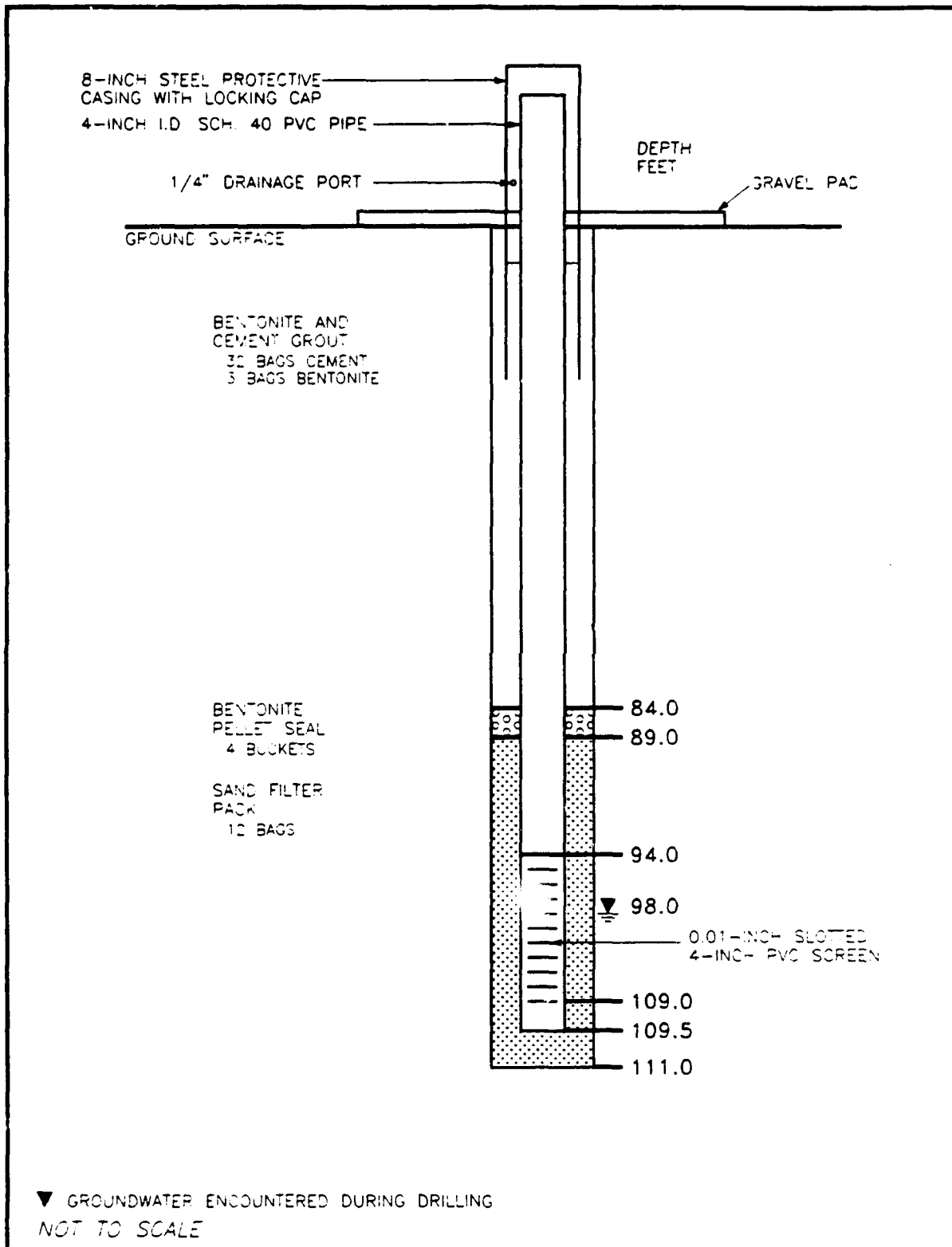
**Well Installation Diagram
Explosive Washout Lagoons
Supplementary Remedial Investigation
UMATILLA, OREGON**

Location: 4-22
Installation Date: 12/09/92
Surface Elevation: 514.80 Feet MSL
Top of PVC Elevation: 516.58 Feet MSL



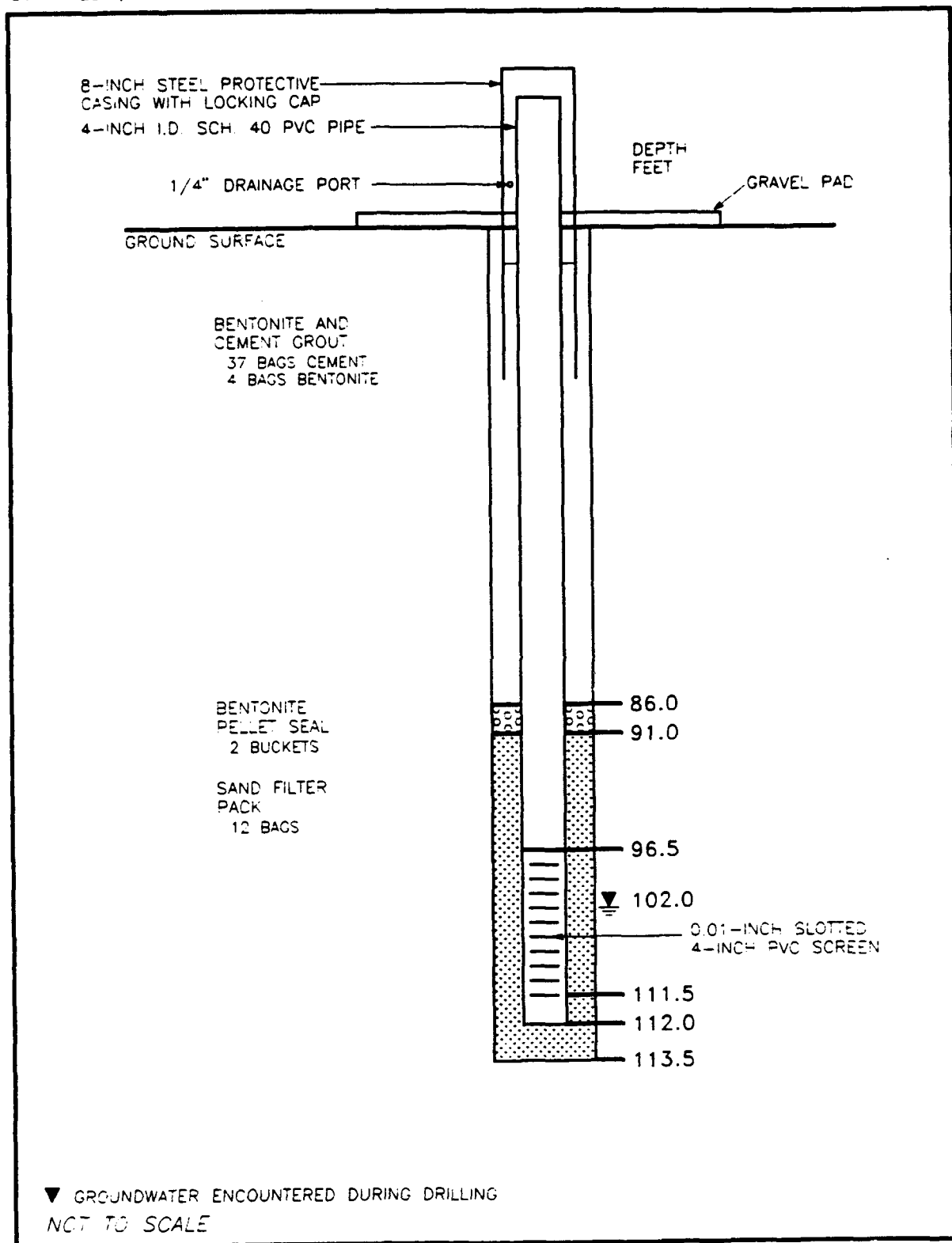
Well Installation Diagram
Explosive Washout Lagoons
Supplementary Remedial Investigation
UMATILLA, OREGON

Location: 4-23
Installation Date: 11/15/92
Surface Elevation: 593.40 Feet MSL
Top of PVC Elevation: 595.34 Feet MSL



Well Installation Diagram
Explosive Washout Lagoons
Supplementary Remedial Investigation
UMATILLA, OREGON

Location: 4-24
Installation Date: 11/15/92
Surface Elevation: 596.50 Feet MSL
Top of PVC Elevation: 598.15 Feet MSL



APPENDIX C
Packer Test Data

max permissible $p_i = 80 \text{ psi}$

Page 1 of 1

Angle

90°

Dealing

Date Started

12/6/92

Due Completed

Ground Elevation _____

Rock Elevation

Groundwater Depletion

Improve it

$$\Sigma k_{Av} = 0.16 \frac{\text{St}}{\text{day}}$$

Gage - Column - Friction Losses Not Pressure
+ height of gage above ground

* Column pressure = (depth to upper packer or depth to groundwater, whichever is smaller) X (0.433)

Conversion factors:

cu.ft x 7.48 gallons

$$Q = f_{bw} \quad (\text{ft}^3/\text{min})$$

$L = \text{Legit} = 6'$

H: Head =

رأى في ذلك

$$K = \frac{G}{2\pi LH} \ln \frac{L}{r} \quad (L > 10r)$$

C-2

Packer Calibration (2178' String)

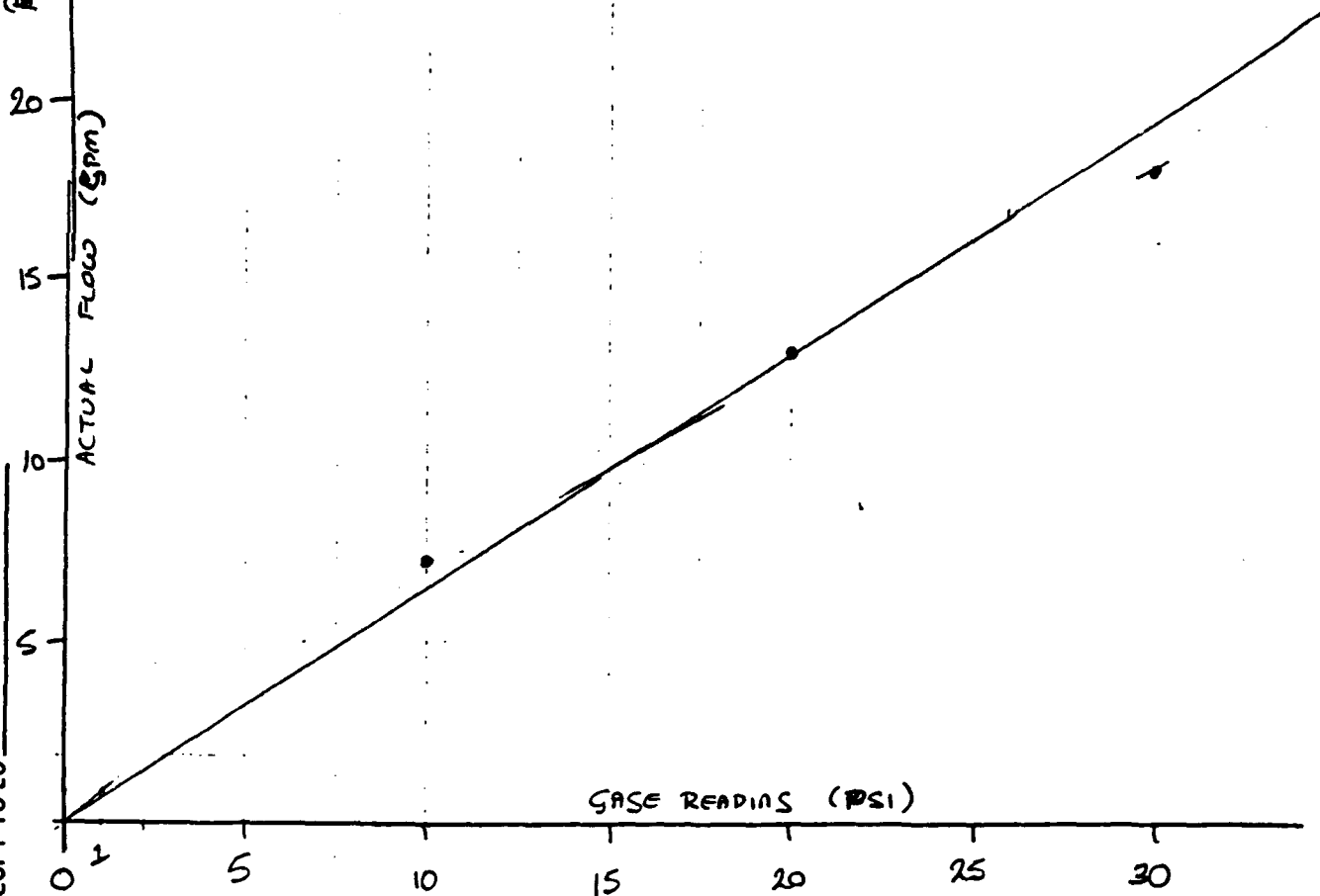
<u>Totalizer Reading</u>	<u>Actual Flow</u>	<u>PSI</u>
16 gpm	18.3 gpm	30
9.7 gpm	13.2 gpm	20
3.6 gpm	7.3 gpm	10

REVISIONS

BY _____ DATE _____ TO EO _____
 BY _____ DATE _____ TO EO _____

Flow (Actual)

BY _____ DATE _____
 CHECKED BY _____
 COPY TO EO _____



PSI

REPORT OF WATER PRESSURE TESTING

Serial No. 4-22
Page 1 of 1

PS1 gage 5.5' above ground Page 1 of 1

Location _____ Angle 90° Ground Elevation -

Coordinates: N _____ Bearing _____ Rock Elevation 55'

E _____ Date Started 12/8/92 Groundwater Elevation 48'

Due Completed _____ Logged by TML / MAO

Test No.	Depth in Feet		Length of Interval Tested	Meter		Water Loss cu. ft. gal.	Elapsed Time (min.)	Rate of Loss $\frac{cu. ft.}{min.}$	Pressure			Net Well	H (feet) (psi. \div .25)	K $\frac{F.T./min.}{\text{---}}$
	From	To		Start (inches in a den.)	End (inches in a den.)				Gauge in psi	P _{in} (-) "Column	P _{out} (-) Friction			
1	79	85	6'	0.06	.1	0.04	1	0.04	10	23.2	0	33.2	76.7	0.08
				.1	.15	0.05	2	0.05	10	23.2	0	33.2	}	
				.15	.17	0.02	3	0.02	10	23.2	0	33.2		
				.17	.18	0.01	4	0.01	10	23.2	0	33.2		
				.18	.19	0.01	5	0.01	10	23.2	0	33.2		v
2	79	85	6'	.20	.20	0	1	0	20	23.2	0	43.2	99.8	0
				.20	.20	0	2	0	20	23.2	0	43.2	}	0
				.20	.20	0	3	0	20	23.2	0	43.2		v
3	79	85	6'	.25	.26	0.01	1	0.01	40	23.2	0	63.2	145.9	0.01
				.26	.30	0.04	2	0.04	40	23.2	0	63.2	}	
				.30	.32	0.02	3	0.02	40	23.2	0	63.2		
				.32	.33	0.01	4	0.01	40	23.2	0	63.2		
				.33	.35	0.02	5	0.02	40	23.2	0	63.2		v
								</						

Depth to groundwater 48' $\text{feet} \times 0.433 =$ 20.78 psi Gage = Column + Friction Loss + Net Pressure
= Column pressure = (depth to upper marker or depth to groundwater, whichever is smaller) \times (0.433) + Gage height

Conversion factors:
cu.ft X 7.48 gallons

Q = flow (m^3/min)
 L = length
 H = Head
 r = hole radius (119)

$$K = \frac{G}{2\pi LH} \ln \frac{L}{r} \quad (L > 10r)$$

1964 100, 120.

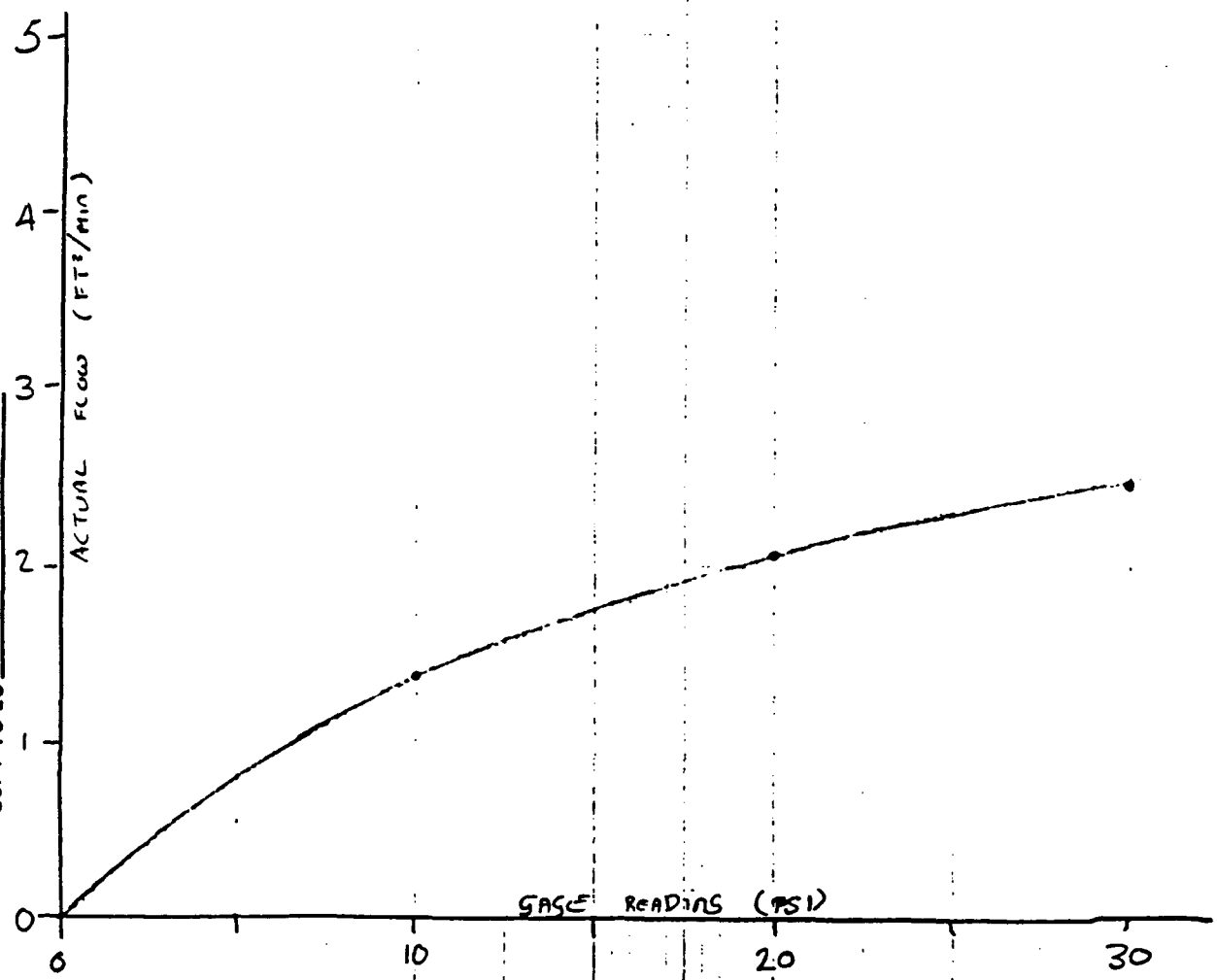
C-4

Packer String Calibration — 82' Packer String

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Flow (ft)		ft = 171" ft = 2.76 (ft)	Elapsed Time (min)	ft/min	Psi gage
Start	End				
0.30	1.05	$0.75 \times 2.76 = 2.07$	1	2.07	20
1.30	1.80	$0.5 \times 2.76 = 1.38$	1	1.38	10
0.25	1.15	$0.9 \times 2.76 = 2.48$	1	2.48	30

BY DATE
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APPENDIX D

Field Parameters (Temperature, Specific Conductance, pH)

WELL DEVELOPMENT RECORDS FOR SITE 4 WELLS

Well Number	Development Date	Water Level Prior to Development (feet T.O.C.)	Actual Total Purge Volume (gal) (Target Purge Volume - gal) (a)	Field Parameters			
				Measure No. (b)	pH	Temp. (C)	Conductivity (uMHOS)
4-19	12-15-92	112.57	325 (252.40)	T1	7.76	17.2	420
				T2	7.43	17.8	400
				T3	7.57	17.8	440
				T4	7.53	17.2	400
				T5	7.49	17.2	380
				T6	7.46	16.7	370
4-20	12-16-92	145.50	350 (332.65)	T1	8.27	18.9	495
				T2	8.96	17.2	375
				T3	7.87	16.1	320
				T4	7.66	16.7	300
				T5	7.55	16.7	300
				T6	7.54	16.7	300
4-21	12-16-92	153.92	290 (283.90)	T1	7.92	18.9	440
				T2	7.71	16.7	400
				T3	7.30	16.1	340
				T4	7.29	16.7	330
				T5	7.31	16.7	330
4-22	12-15-92	58.35	260 (253.80)	T1	7.79	17.2	240
				T2	7.40	16.7	300
				T3	7.12	16.7	320
				T4	7.56	16.7	300
				T5	7.55	16.7	310
4-23	11-19-92	100.62	180 (102.35)	T1	7.37	13.4	412
				T2	7.14	12.9	342
				T3	7.20	12.9	312
				T4	7.17	13.1	332
				T5	7.20	13.1	330
				T6	7.21	13.2	327
4-24	11-19-92	103.60	125 (84)	T1	7.72	12.9	439
				T2	7.57	12.6	366
				T3	7.50	12.6	327
				T4	7.51	12.7	333
				T5	7.52	12.6	332

(a) Target purge volume calculated is five pore volumes.

(b) Measurement T1 was taken from the first water that was removed from the well. The last measurement listed was taken within approximately fifteen minutes of the end of purging (i.e., from some of the last water removed from the well).

APPENDIX E

Slug Test Data

SLUG TEST CALCULATIONS **INTERMEDIATE WELLS 4-19, 4-20, 4-21, AND 4-22**

Cooper Slug Test Calculations**

<u>Well No.</u>	<u>K (ft/day)</u>	<u>D (ft)</u>	<u>rw (ft)</u>	<u>rc (ft)</u>	<u>t (sec)</u>	<u>B</u>	<u>A</u>
4-19	277	10	0.33	0.17	0.9	1.0	0.1
4-20	416	10	0.33	0.17	0.6	1.0	0.1
4-21	624	10	0.33	0.17	0.4	1.0	0.001
4-22	357	10	0.33	0.17	0.7	1.0	0.1

** Input quantities are as follows:

D = Length of screen

rw = Radius from center of well to undisturbed aquifer material

rc = Casing diameter

t = Time from plot of drawdown vs. time corresponding to B=1 on type curve

B = Type curve value for KDt/r^2c

A = Type curve value for r^2wS/t^2c

Cooper Method Calculations

$$KD = \frac{r_c^2 \beta}{t} \quad S = \frac{r_c^2 \alpha}{r_{ew}^2}$$

4-19

$$r_c = 0.17$$

$$D = 10.0$$

$$\beta = 1.0$$

$$r_{ew} = 0.33$$

$$t = 0.9$$

$$\alpha = 0.1$$

$$K = \frac{(0.17)^2 \cdot 1}{0.9 \cdot 10} = 3.21 \times 10^{-3} \text{ ft/sec}$$

$$277.44 \text{ ft/day}$$

$$S = \frac{(0.17)^2 \cdot 0.1}{(0.33)^2} = 2.65 \times 10^{-2}$$

4-20

$$r_c = 0.17$$

$$D = 10.0$$

$$\beta = 1.0$$

$$r_{ew} = 0.33$$

$$t = 0.6$$

$$\alpha = 0.1$$

$$K = \frac{(0.17)^2 \cdot 1}{0.6 \cdot 10} = 4.85 \times 10^{-3} \text{ ft/sec}$$

$$416.16 \text{ ft/day}$$

$$S = \frac{(0.17)^2 \cdot 0.1}{(0.33)^2} = 2.65 \times 10^{-2}$$

4-21

$$r_c = 0.17$$

$$D = 10.0$$

$$\beta = 1.0$$

$$r_{ew} = 0.33$$

$$t = 0.4$$

$$\alpha = 0.001$$

$$K = \frac{(0.17)^2 \cdot 1}{0.4 \cdot 10} = 7.23 \times 10^{-3} \text{ ft/sec}$$

$$624.24 \text{ ft/day}$$

4-22

 $r_c = 0.17$ $D = 10.0$ $\beta = 1.0$ $r_{ew} = 0.33$ $L = 0.7$ $\alpha = 0.1$

$$K = \frac{(0.17)^2 \cdot 1}{0.7 \cdot 10} = 4.13 \times 10^{-3} \text{ ft/sec}$$

$$356.71 \text{ ft/day}$$

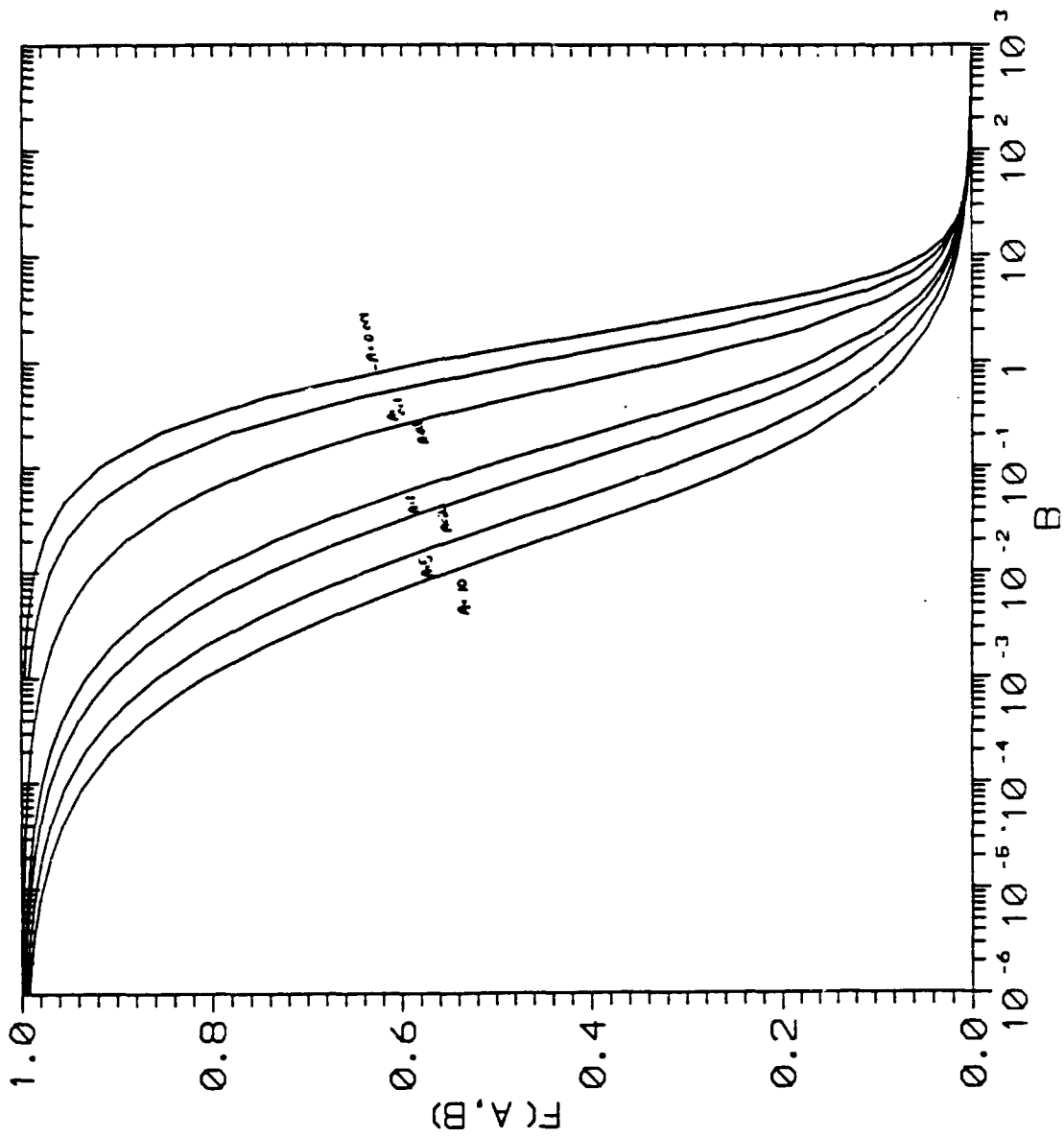
$$S = \frac{(0.17)^2 \cdot 0.1}{(0.33)^2} = 2.65 \times 10^{-2} \text{ ft.}$$

REVISIONS

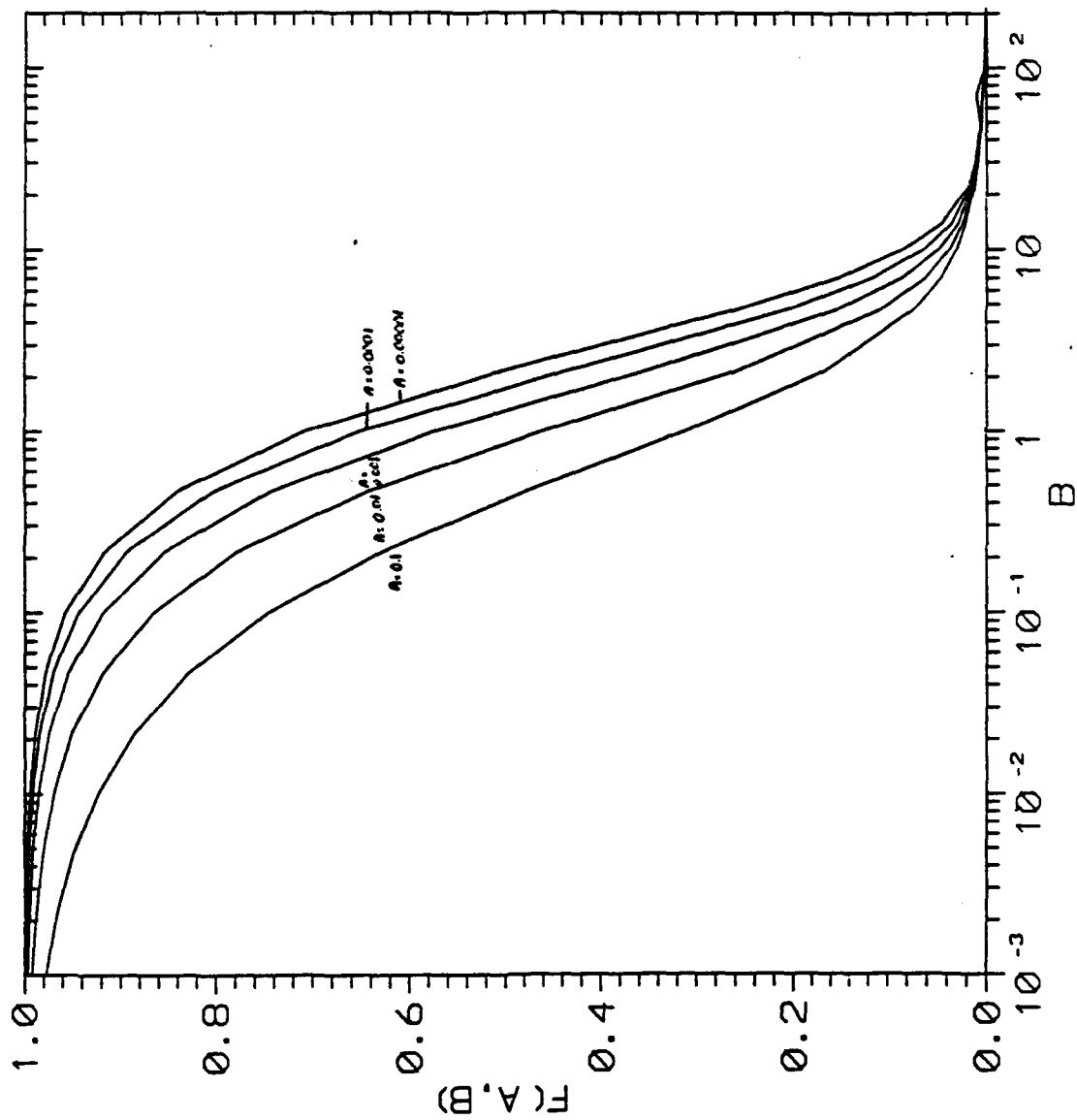
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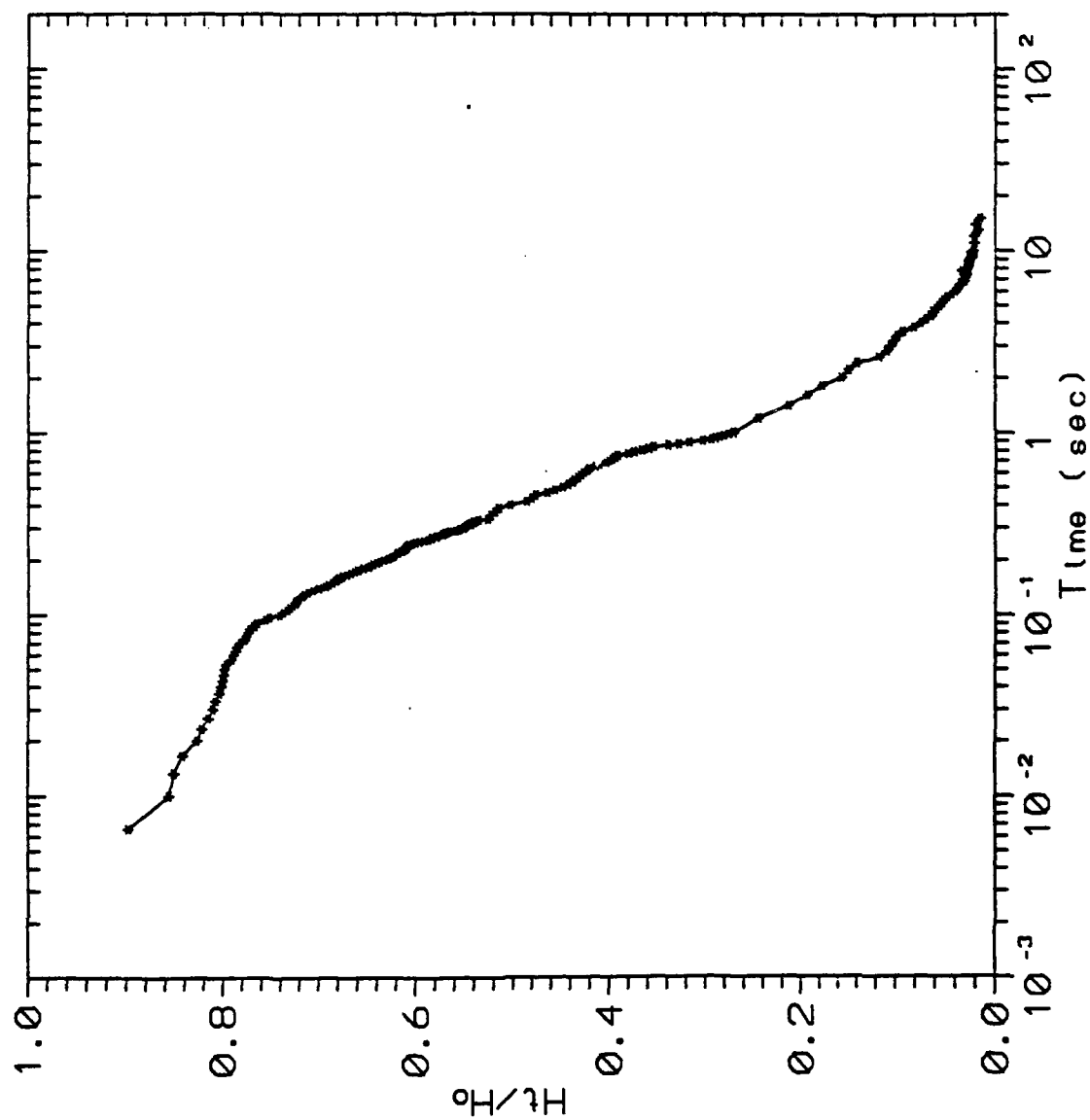
COOPER TYPE CURVES



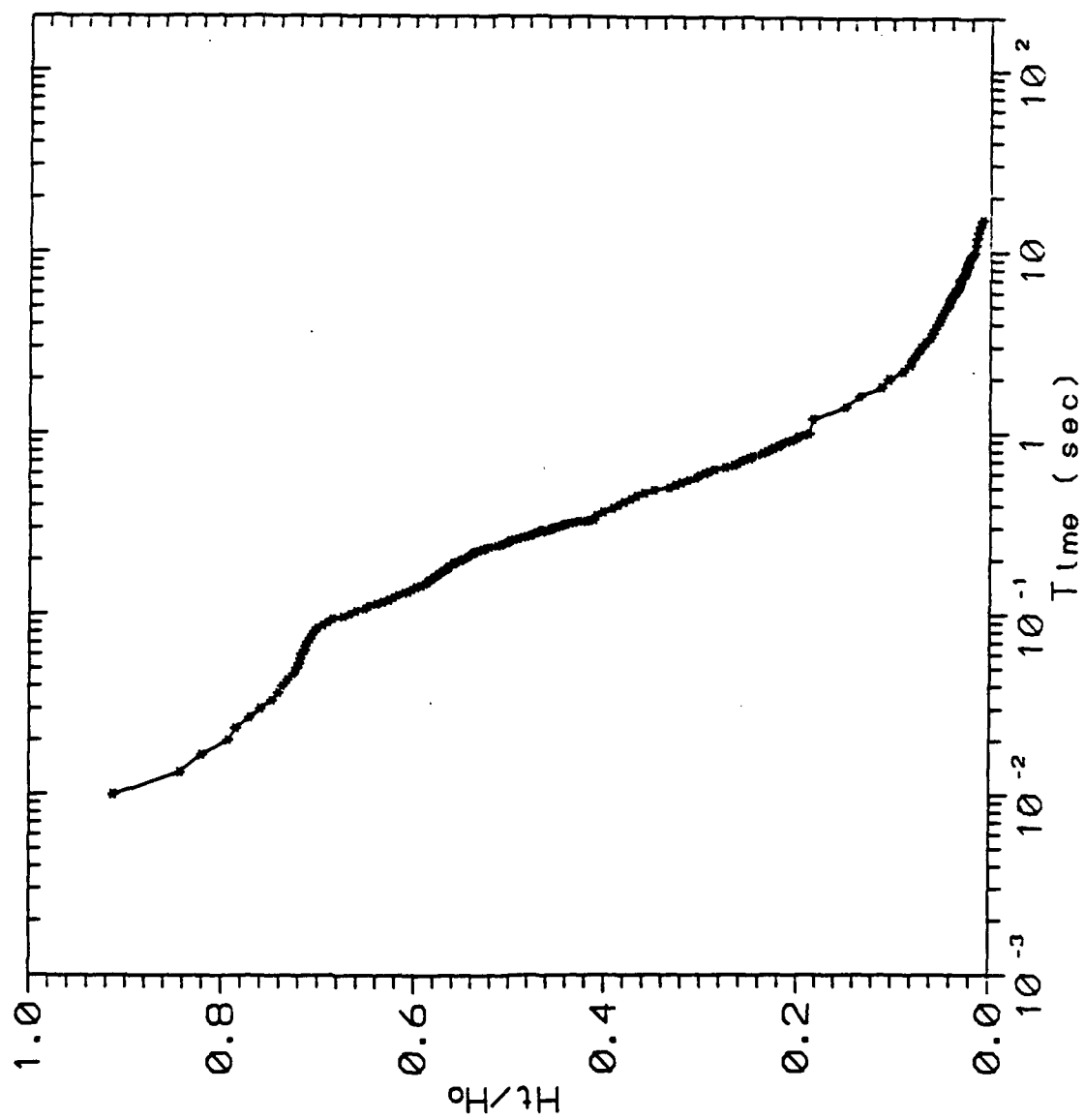
COOPER TYPE CURVES
 $10^{-5} < A < 10^{-1}$



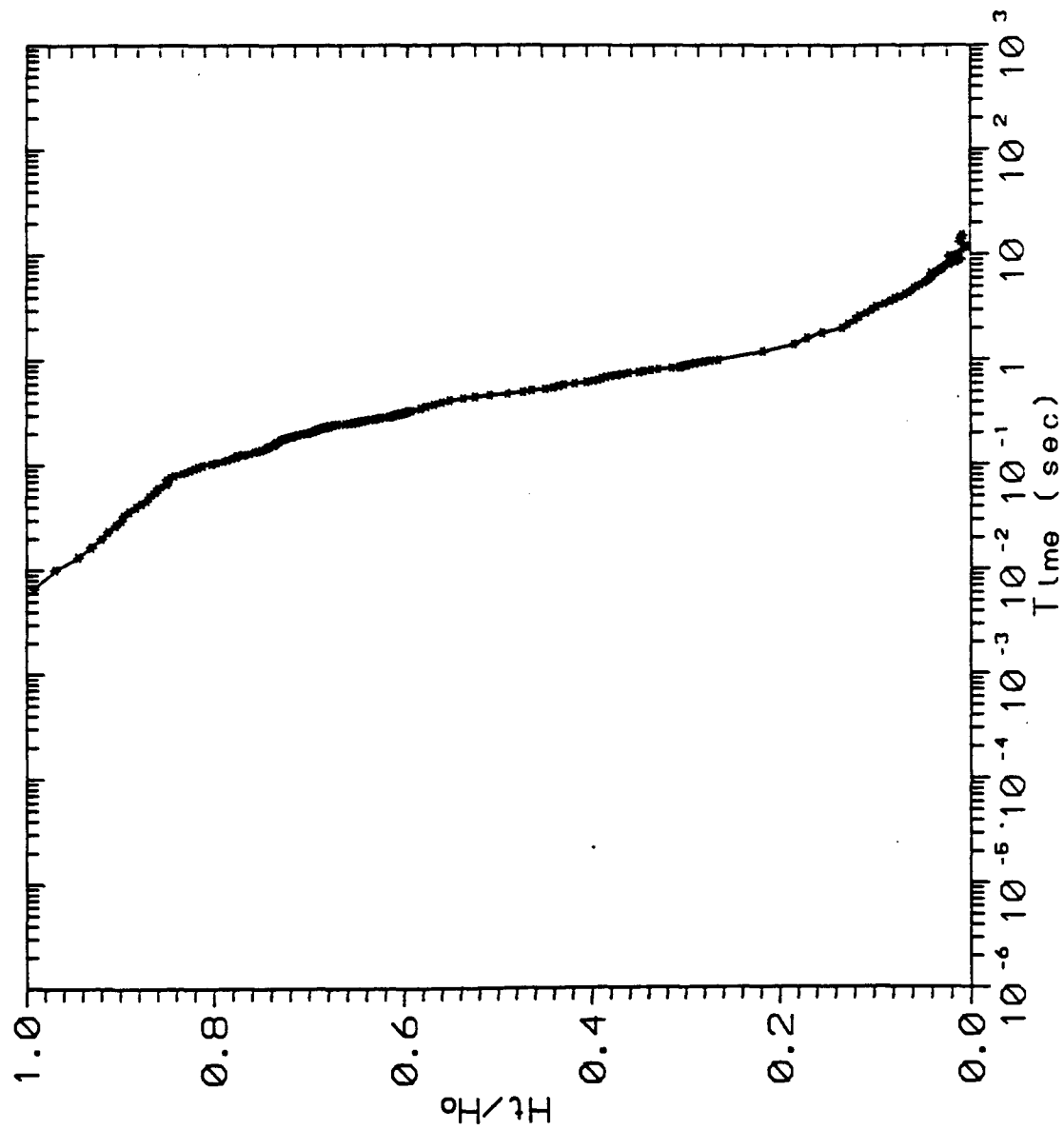
UMATILLA SLUG TEST DATA FOR 4-19



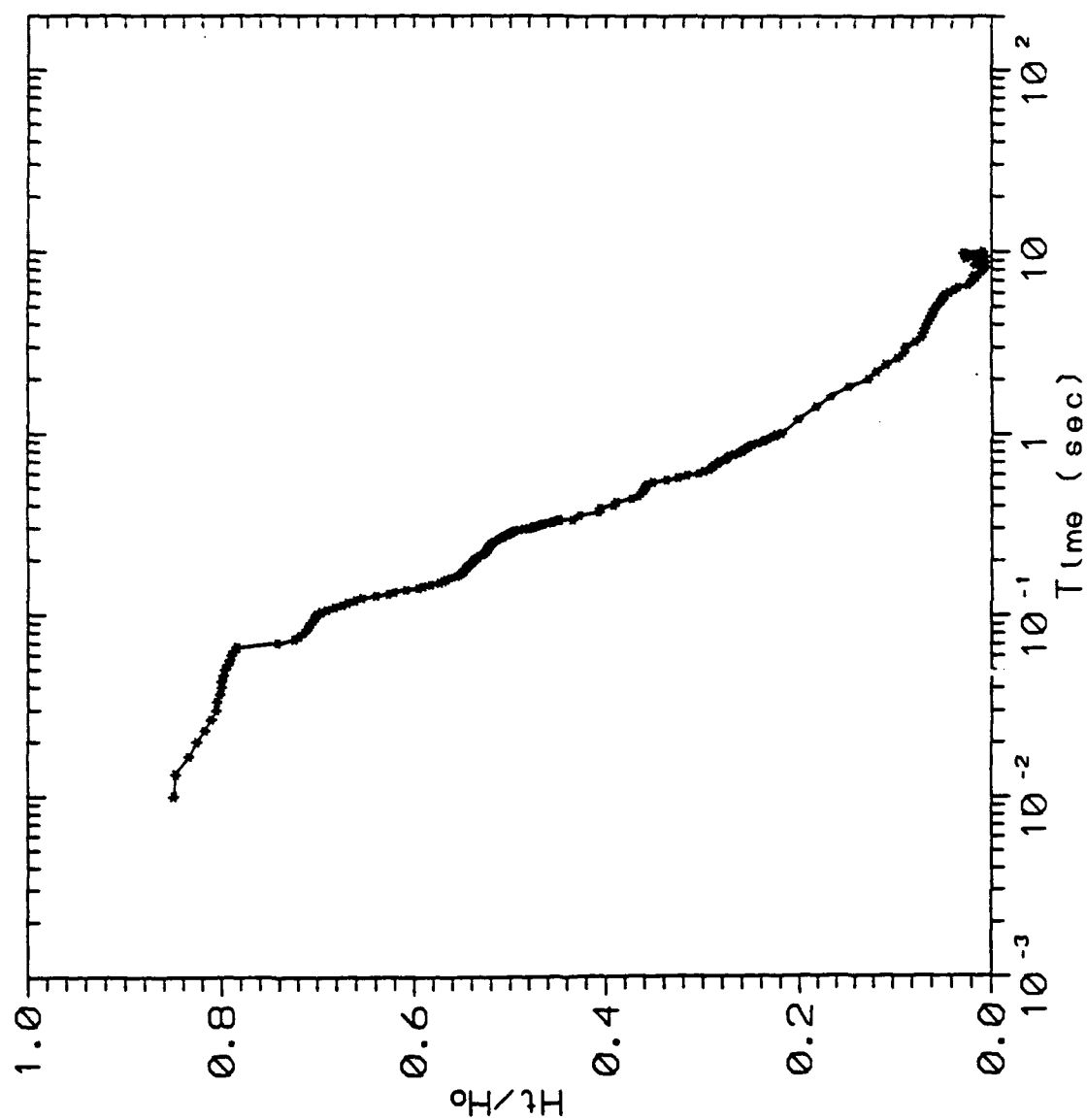
UMATILLA SLUG TEST DATA FOR 4-20



UMATILLA SLUG TEST DATA FOR 4-21



UMATILLA SLUG TEST DATA FOR 4-22



SLUG TEST CALCULATIONS **ALLUVIAL WELLS 4-23 AND 4-24**

Bouwer and Rice Slug Test Model Calculations*

<u>Well No.</u>	<u>K (ft/day)</u>	<u>D (ft)</u>	<u>H (ft)</u>	<u>L (ft)</u>	<u>rw (ft)</u>	<u>rc (ft)</u>	<u>t (sec)</u>	<u>y0 (ft)</u>	<u>yt (ft)</u>
4-23	1571	8.55	8.55	15	0.38	0.24	0.2	0.07	0.032
4-24	1944	8.05	8.05	15	0.38	0.24	0.45	0.055	0.006

* Input quantities are as follows:

D = Depth from water table to base of aquifer (saturated thickness)

H = Depth from water table to bottom of screen

L = Length of screen

rw = Radius from center of well to undisturbed aquifer material

rc = Casing diameter plus a correction for the presence of a gravel or sand pack

t = Arbitrary time selected to pick value of yt from straight-line portion of plot of drawdown vs. time

y0 = Drawdown at point where the extended straight-line portion of the graph intersects the y-axis at zero time

yt = Drawdown at time t on the straight-line portion of the graph

Bouwer and Rice Method Calculations

$$K = \frac{r_c^2 \ln(r_w/r_c)}{2L} \cdot \frac{1}{t} \cdot \ln\left(\frac{y_0}{y_e}\right) \quad \ln \frac{r_w}{r_c} = \left[\frac{1.1}{\ln(r_w/r_c)} + \frac{C}{L/r_w} \right]^{-1}$$

$$\text{Correction for } r_c = [r_a^2 + n(r_w^2 - r_a^2)]^{1/2}$$

4-23

H = 8.55

t = 0.2

r_a = 0.17

L = 15.0

y_0 = 0.07

n = 25%

r_w = 0.38

y_e = 0.032

r_c = 0.24

C = 2.39

$$r_c = [0.17^2 + 0.25(0.38^2 - 0.17^2)]^{1/2} = 0.24$$

$$\ln \frac{r_w}{r_c} = \left[\frac{1.1}{\ln(r_w/r_c)} + \frac{2.39}{15/0.38} \right]^{-1} = 2.42$$

$$K = \frac{0.24^2 \cdot 2.42}{2 \cdot 15.0} \cdot \frac{1}{0.2} \cdot \ln\left(\frac{0.07}{0.032}\right) = 1.82 \times 10^{-2} \text{ ft/sec}$$

1571.19 ft/d

4-24

H = 8.05

t = 0.45

r_a = 0.17

L = 15.0

y_0 = 0.055

n = 25%

r_w = 0.38

y_e = 0.006

r_c = 0.24

C = 2.39

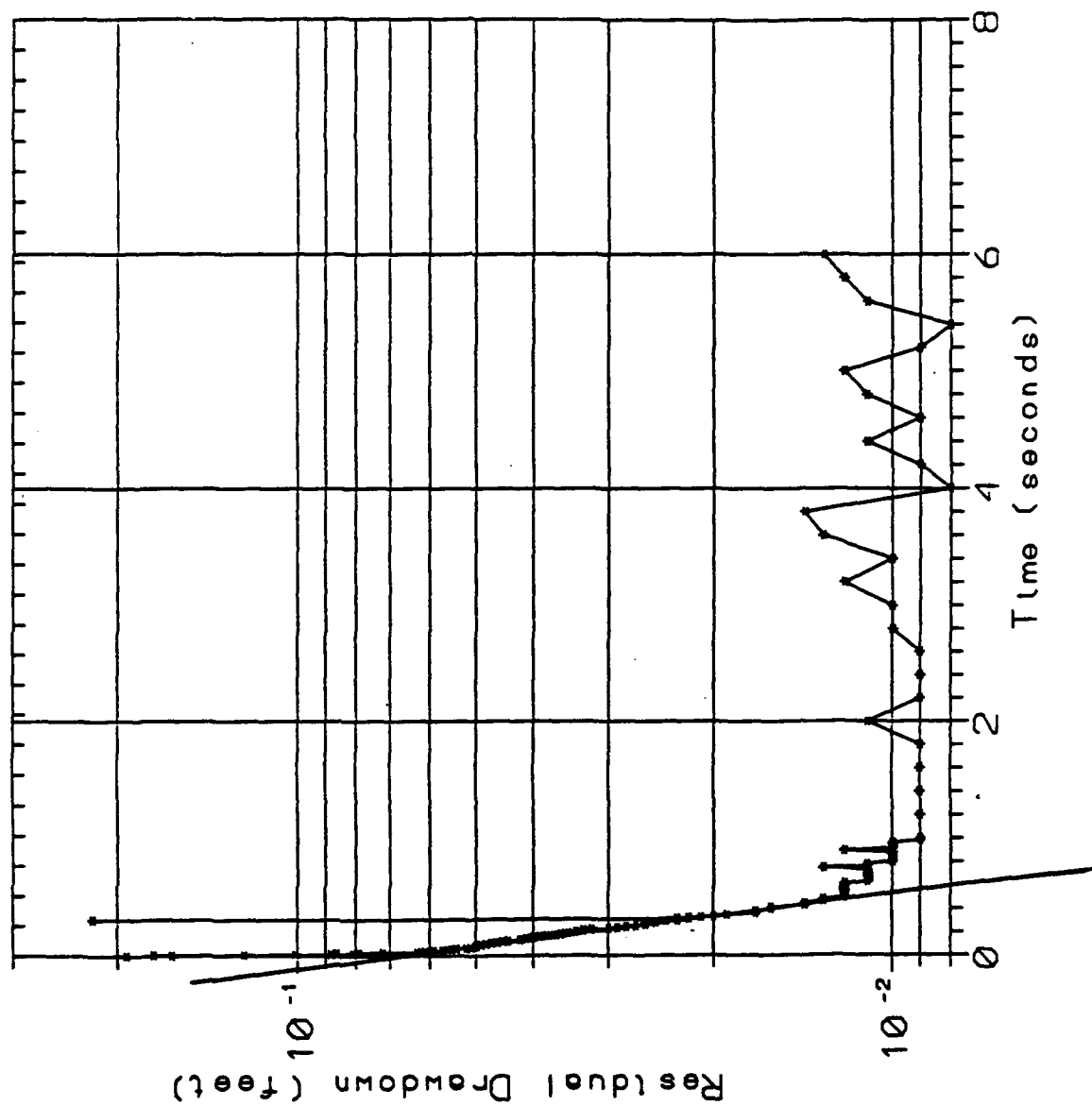
$$r_c = [0.17^2 + 0.25(0.38^2 - 0.17^2)]^{1/2} = 0.24$$

$$\ln \frac{r_w}{r_c} = \left[\frac{1.1}{\ln(r_w/r_c)} + \frac{2.39}{15/0.38} \right]^{-1} = 2.38$$

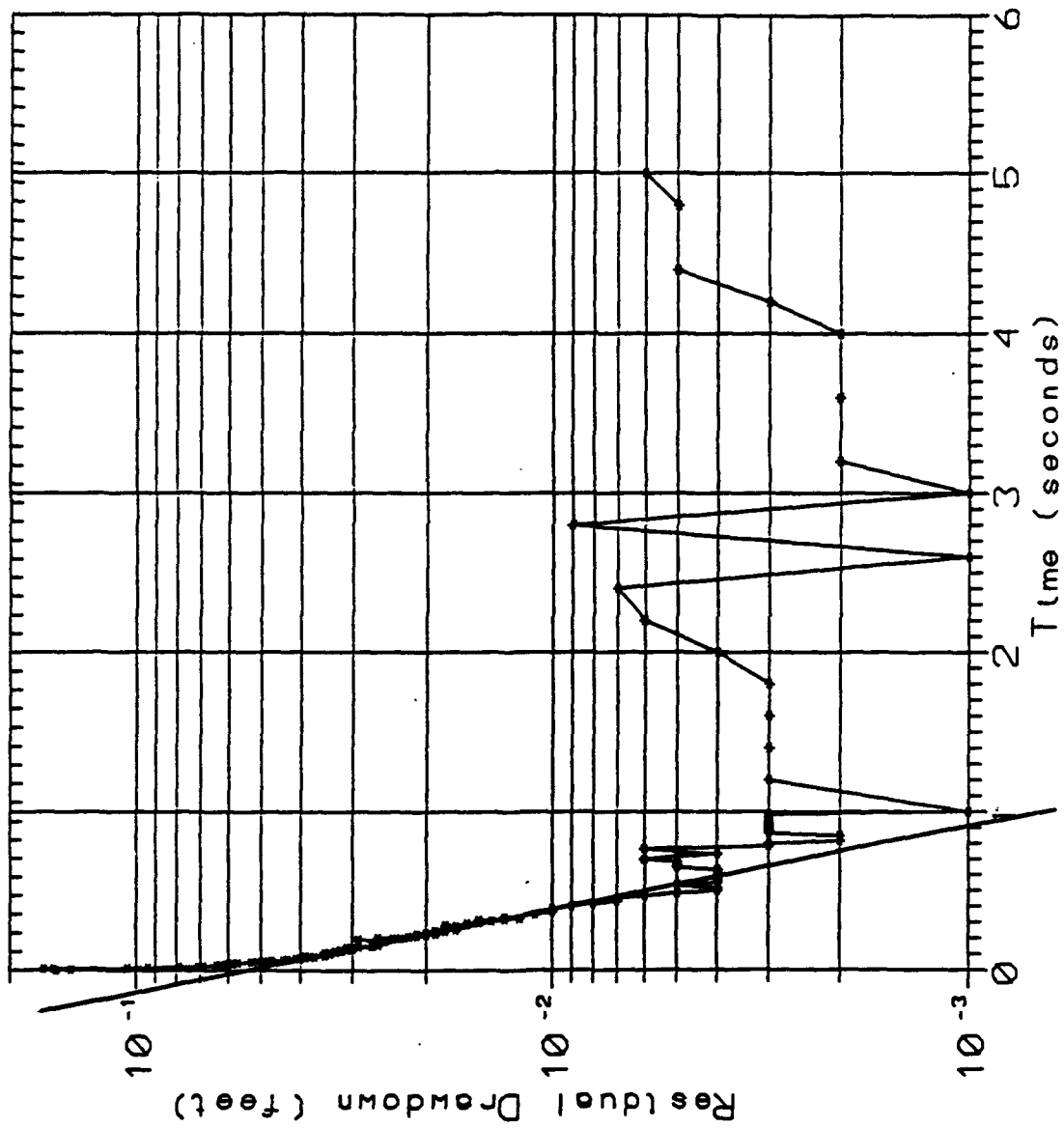
$$K = \frac{0.24^2 \cdot 2.38}{2 \cdot 15} \cdot \frac{1}{0.45} \cdot \ln\left(\frac{0.055}{0.006}\right) = 2.25 \times 10^{-2} \text{ ft/sec}$$

1943.86 ft/d

UMATILLA SLUG TEST DATA FOR 4-23



UMATILLA SLUG TEST DATA FOR 4-24



APPENDIX F

XRF Analytical Results of Basalt Core Samples

Mark Ochsner
Dames and Moore
1750 S.W. Harbor Way, Suite 400
Portland, OR 97201

February 22, 1993

Dear Mark:

The X-ray fluorescence (XRF) analyses for the Umatilla-Ordinance Depot samples 4-20 (170-176.5') and 4-22 (75-80') just received from Washington State University's GeoAnalytical Laboratory are enclosed. Both of these samples are Elephant Mountain Member of the Saddle Mountains Basalt. The chemistry is an excellent match for Elephant Mountain and the lithology is also consistent, being abundantly microphyric with larger phenocrysts rare. Chemically the lower SiO_2 , intermediate P_2O_5 , and higher TiO_2 abundances are distinctive. This unit is usually underlain by the Rattlesnake Ridge interbed.

I checked the magnetic polarity using top and bottom of the core samples with a flux-gate magnetometer and found the sample from 4-22 to read "reversed" while the sample from 4-20 read "normal". Perhaps one of the cores had been inverted in handling, but Elephant Mountain is considered to be "reversed" to "transitional" paleomagnetic polarity.

Elephant Mountain Member comprises two flows in some of its distributional area, but the Umatilla location is very near to the mapped edge of this unit. The other reversed polarity unit that also pinches out in this locality is the Pomona Member, but these chemical analyses are nothing like the Pomona composition. Therefore, I can confidently conclude that these two core samples are from the Elephant Mountain Member of the Saddle Mountains Basalt.

Thank you for the opportunity to consult with you on this project! If you have any questions or need further consultation, please give me a call.

Sincerely,



Marvin H. Beeson, Ph.D.
Geologist (OR G493)

Table of XRF Data

UMATILLA-ORDINANCE DEPOT

Drill Hole	4-20	4-22
Depth	170-175'	75-80'
XRF Date	17-Feb-93	17-Feb-93

Normalized Results (Weight %)

SiO2	51.16	50.33
Al2O3	12.86	12.75
TiO2	3.55	3.49
FeO*	14.91	14.34
MnO	0.215	0.30
CaO	8.60	9.95
MgO	4.41	4.37
K2O	1.15	1.14
Na2O	2.60	2.79
P2O5	0.538	0.538

Trace Elements (ppm)

Ni	4	6
Cr	23	20
Sc	39	35
V	412	424
Ba	467	459
Rb	28	28
Sr	235	240
Zr	239	236
Y	51	50
Nb	26.4	27.3
Ga	22	19
Cu	15	11
Zn	148	144
Pb	6	3
La	29	34
Ce	78	72
Th	6	8

CRBG	Elephant	Elephant
UNIT	Mountain	Mountain

Major elements are normalized on a volatile-free basis
 *Total Fe is expressed as FeO

XRF Analyses by WSU GeoAnalytical Laboratory